# Technical Memorandum 

To: John Tully, Deputy Commissioner, Putnam County Highways \& Facilities<br>From: Michael Wieszchowski, PE, PTOE, Greenman-Pedersen, Inc.<br>Subject: Roundabout Supplemental Analysis Summary<br>Date: October 3,2019

To supplement the Traffic Analysis and Roundabout Feasibility Report prepared in June 2019, additional analysis was performed at the following 3 intersections.
9. Fairfield $\operatorname{Dr}$ \& Haviland Dr
10. Fairfield $\operatorname{Dr} \&$ Haviland $\operatorname{Dr}$
11. Secor Rd \& Wood St

A summary of each evaluation is as follows:

## Fairfield Dr \& Haviland Dr

- Level of Service and Capacity appear adequate for the traffic volumes present in the peak hours.
- Neither traffic volumes nor accidents are sufficient enough to warrant a traffic signal.
- Vehicles backing from roadside parking stalls into the travelway appear to be a significant contributor to the high accident rate at this location.
- Sight distance is less than desirable, but not critically limited.
- A Roundabout would require significant property acquisition and even then slopes would make installation difficult. A roundabout is not recommended for this location.
- Two concepts are presented in the Report that could improve safety at this location, both require significant coordination and "Buy-in" of property owners to reconfigure parking.


## Fairfield Dr \& Haviland Dr

- Level of Service and Capacity appear adequate for the traffic volumes present in the peak hours. Although there is a potential queuing issue eastbound which could impact safety.
- Neither traffic volumes nor accidents are sufficient enough to warrant a traffic signal.
- Accident rate is high, but no pattern of concern was noted. Contributing factors could potentially be adjacent roadside parking backing out into the travelway or sight distance limitation along Haviland Dr looking left past the war memorial, but neither of these factors were listed as a factor in any of the accidents reported.
- A Roundabout would require significant property acquisition and even then the approaching slope on Haviland Dr may make installation difficult. A roundabout is not recommended for this location.
- Two concepts are presented in the Report that could improve safety and reduce queues at this location, both require significant coordination and "Buy-in" of property owners to eliminate roadside parking spaces in order to construct an eastbound left turn lane.


## Secor Rd \& Wood St

- Level of Service and Capacity appear adequate for the traffic volumes present in the peak hours.
- Neither traffic volumes nor accidents are sufficient enough to warrant a traffic signal.
- Accident rate is high, and although there is no definitive correctable pattern of accidents, there is a higher than normal percentage of right angle crashes. Given the all-way stop condition, this should not occur unless drivers are not seeing or ignoring the stop signs.
- A Roundabout could be constructed within the existing right-of-way at this location. Although not warranted by traffic volume at this time, the installation of a roundabout would eliminate the possibility of right angle accidents which should improve safety.

The evaluation sheets, data sheets, conceptual cost estimate and concept sketches for each intersection follows:

## SUMMARY OF INTERSECTION EVALUATION TOWNERS RD AND HILL AND DALE RD/LAKESHORE DR

## Existing Conditions:

The existing intersection has four approaches with Towner Rd approaching from the northwest and northeast, curving significantly within the intersection and being uncontrolled. Hill and Dale Road approaches from the south and Lakeshore Driver approaches from the north and both are stop sign controlled. On the south side of the intersection there is a deli and an auto repair shop that have wide curb cuts that run the length of their frontage and cars are allowed to park in front of the businesses. This is problematic as car's pulling out of these parking spaces have to back into the roadway in order to get out of the properties. This situation also occurs on the north side for a newly renovated hair salon and gift shop building. There are no pedestrian crossing accommodations at the intersection and there are no sidewalks approaching the intersection. It should also be noted that there is a significant downgrade on the north side of the intersection, with slopes of $10 \%$ or more leading away from the intersection.
Sight distance is limited by both horizontal and vertical curvature, as well as parked vehicles at the deli for both side streets. It appears that there is sufficient stopping sight distance for the 30 mph speed limit (200 foot minimum), but in some area's the 335 feet needed for desirable intersection sight distance is not available.

A traffic analysis was conducted and capacity is adequate at this intersection. Intersection Level of service is LOS A in both peak hours and no approach operates worse than LOS B. An Intersection Evaluation worksheet, showing geometric details, the existing traffic volumes, and a summary of the capacity analyses is attached.

## Signal Warrant Analysis:

A review of the hourly traffic volumes between 7:00 AM and 8:00 PM show that none of the warrants reviewed; Warrant 1 (8-hour warrant), Warrant 2 (4-hour warrant) or Warrant 3 (peak hour warrant) are satisfied for the existing traffic volumes. In fact, there is not a single hour that satisfies the minimum requirements for the least restrictive 8 -hour warrant. Additionally, fewer than 5 accidents per year occur at this location, so Warrant 7 (Crash Experience) is not satisfied either. With no warrants being satisfied, a traffic signal, or similar treatment such as a roundabout, is not justified. See attached signal warrant analysis worksheets for more details.

## Accident Analysis:

Accident data shows 10 accidents at this location in the 3-year period (2016-2018) reviewed. This results in an accident rate of 1.82 accidents/MEV, which is 5 times the statewide average for similar intersections. However, the majority of the accidents (60\%) had nothing to do with the intersection and were related to the parking situation adjacent to the intersection and vehicles backing out into the roadway. Outside of that, there is no accident pattern that would be of concern. The accidents types and severity are summarized in the table below, and accident records are attached.

ACCIDENT SUMMARY

| Accident Type | Number of Occurrences | Accident Severity | Number of Occurrences |
| :--- | :---: | :--- | :---: |
| Right Angle | 3 (all 3 involving backing) | Fatality | 0 |
| Sideswipe | $3(1$ involving backing) | Personal Injury | 2 |
| Rear End | $2(1$ involving backing) | Property Damage Only | 3 |
| Pedestrian | 1 | Non-Reportable | 5 |
| Other | 1 (Involved backing) |  |  |
|  | 10 |  | 10 |
|  |  |  |  |

## Field Condition and Right of Way Review:

This location is not conducive to the installation of a roundabout. The significant slopes to the north of the intersection would require the roundabout to be constructed more to the south, so any roundabout solution would require acquisition and demolition of both the Deli and the Auto Repair shop to the south of the intersection, and even then, the slopes to the north would be difficult to address leading into a roundabout.

## Design Alternative Consideration:

As there is no existing capacity issue with the current geometry, alternatives that included the installation of a traffic signal and a roundabout were analyzed for informational purposes but were not considered as reasonable alternatives. With both a traffic signal and roundabout, the intersection would operate at LOS A, same as the existing condition, so neither provides a significant level of service benefit either. Figure 9 does depict the roundabout option in order to show the construction footprint and right-of-way impacts, but as mentioned, it isn't warranted and would require the demolition of two key area businesses. As such, two other improvement options were considered. Both keeping the existing traffic control, but better addressing the safety issues identified at this location.

Concept A keeps the roadway as it is and only reconfigures parking to removes vehicles backing into the mainline traffic. It does this by moving the deli parking to the side road and constructing a retaining wall deeper into the northern property to allow enough room for vehicle turnouts without hitting the road. See Figure 9A for a concept sketch of this alternative. With this option, there will still be vehicles backing into a roadway at the deli, but they will be backing into a very lightly traveled local road, which poses far less of a safety concern than backing out onto Towners Road. This option would require significant cooperation and coordination with the business owners, but would provide a much safer condition than the existing geometry.
Concept B takes a similar approach, but also realigns Towners Rd to provide less curvature and better sight distance. Treatment on the north side would be similar to Concept A, but with the roadway shifting to the north, it allows parking to remain in front of the deli by providing more maneuvering space (see Figure 9B). This option still requires "buy-in" from the business owners, as improvements are being made on private property, and it has significant grade issues to overcome, but is the option that best addresses both sight distance and parking to improve safety.

## Conceptual Cost Estimate:

Based on our past experience with similar projects, knowledge of construction pricing in this region of New York State and our understanding of the issues, it is estimated that Concept A would cost approximately $\$ 800,000$, and concept $B$, with the road realignment, would cost approximately $\$ 1,580,000$. These costs include construction of all improvements, right-of-way, wetland mitigation, and costs for design and inspection. If a roundabout was progressed, it would likely cost close to $\$ 3 \mathrm{M}$ because of the extensive property acquisitions and slope mitigation. Cost estimates with a breakdown of the big picture cost items is attached.

## Summary \& Conclusion:

The analysis shows that there is no capacity or level of service issues at the existing intersection and that the need for more extensive traffic control, such as a signal or roundabout, is not warranted. However, the accident analysis did identify a safety issue with vehicles backing out of adjacent businesses onto the roadway, and sight distance is somewhat limited for the side street traffic. It is recommended that parking adjacent to the intersection be reconfigured in some way to reduce the likelihood vehicles backing into the travelway, similar to that shown in either Concept Sketch A or Concept Sketch B. If this parking reconfiguration could be incorporated with a realignment of Towners Rd, improved sight distance could be achieved, and safety maximized.



Towners Rd \& Hill and Dale Rd

## Carmel Hamlet NY



Towners Rd \& Hill and Dale Rd

## Carmel Hamlet NY



| Towners Rd \& Hill and Dale Rd Carmel Hamlet NY |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Southbound Lakeshore Dr |  |  |  |  | Westbound Towners Rd |  |  |  |  | Northbound Hill and Dale Rd |  |  |  |  | Eastbound <br> Towners Rd |  |  |  |  | TOTAL |
| Time |  | Left Turns | Straight |  | Peds/ |  |  | Straight |  | Peds/ |  |  | Straight | Right | Peds/ |  |  | Straight | Right |  |  |
| Time | Uurns | Left Turns | Through | Turns | Bicycles | U Turns | Left Turns | Through | Turns | Bicycles | Turns | Left Turns | Through | Turns | Bicycles | U Turns | Left Turns | Through | Turns | Bicycles |  |
| 4:00 PM | 0 | 0 | 6 | 10 | 0 | 0 | 4 | 9 | 0 | 1 | 0 | 30 | 10 | 5 | 0 | 0 | 8 | 13 | 15 | 1 | 110 |
| 4:15 PM | 0 | 0 | 5 | 7 | 0 | 0 | 5 | 7 | 0 | 0 | 1 | 38 | 9 | 9 | 0 | 2 | 9 | 14 | 9 | 2 | 115 |
| 4:30 PM | 0 | 0 | 5 | 6 | 0 | 0 | 5 | 11 | 0 | 0 | 0 | 21 | 12 | 10 | 1 | 0 | 9 | 17 | 14 | 0 | 110 |
| 4:45 PM | 0 | 0 | 5 | 4 | 0 | 0 | 4 | 8 | 0 | 0 | 0 | 24 | 10 | 10 | 0 | 0 | 10 | 23 | 21 | 2 | 119 |
| Hourly Total | 0 | 0 | 21 | 27 | 0 | 0 | 18 | 35 | 0 | 1 | 1 | 113 | 41 | 34 | 1 | 2 | 36 | 67 | 59 | 5 | 454 |
| 5:00 PM | 0 | 0 | 4 | 8 | 0 | 0 | 5 | 13 | 3 | 0 | 0 | 30 | 9 | 7 | 0 | 0 | 7 | 19 | 15 | 0 | 120 |
| 5:15 PM | 0 | 0 | 2 | 6 | 0 | 0 | 12 | 8 | 1 | 0 | 0 | 39 | 11 | 13 | 0 | 0 | 7 | 19 | 18 | 0 | 136 |
| 5:30 PM | 0 | 0 | 9 | 11 | 0 | 0 | 7 | 12 | 0 | 0 | 0 | 28 | 6 | 25 | 0 | 0 | 4 | 15 | 20 | 1 | 137 |
| 5:45 PM | 0 | 0 | 6 | 5 | 0 | 0 | 4 | 13 | 1 | 0 | 0 | 25 | 3 | 11 | 2 | 0 | 10 | 13 | 15 | 1 | 106 |
| Hourly Total | 0 | 0 | 21 | 30 | 0 | 0 | 28 | 46 | 5 | 0 | 0 | 122 | 29 | 56 | 2 | 0 | 28 | 66 | 68 | 2 | 499 |
| 6:00 PM | 0 | 0 | 5 | 7 | 0 | 0 | 3 | 15 | 0 | 0 | 0 | 20 | 11 | 7 | 0 | 0 | 5 | 27 | 12 | 3 | 112 |
| 6:15 PM | 0 | 0 | 3 | 5 | 0 | 0 | 6 | 11 | 2 | 0 | 0 | 26 | 9 | 8 | 3 | 0 | 7 | 14 | 14 | 2 | 105 |
| 6:30 PM | 0 | 0 | 2 | 4 | 1 | 0 | 12 | 13 | 0 | 0 | 0 | 23 | 8 | 12 | 0 | 1 | 9 | 13 | 18 | 1 | 115 |
| 6:45 PM | 0 | 0 | 3 | 6 | 0 | 0 | 13 | 17 | 0 | 0 | 0 | 32 | 7 | 10 | 0 | 0 | 5 | 8 | 10 | 0 | 111 |
| Hourly Total | 0 | 0 | 13 | 22 | 1 | 0 | 34 | 56 | 2 | 0 | 0 | 101 | 35 | 37 | 3 | 1 | 26 | 62 | 54 | 6 | 443 |
| 7:00 PM | 0 | 0 | 2 | 8 | 1 | 0 | 13 | 9 | 0 | 0 | 0 | 17 | 10 | 5 | 2 | 0 | 6 | 22 | 14 | 1 | 106 |
| 7:15 PM | 0 | 1 | 4 | 3 | 0 | 0 | 6 | 13 | 0 | 0 | 0 | 13 | 4 | 12 | 2 | 0 | 7 | 12 | 17 | 3 | 92 |
| 7:30 PM | 0 | 0 | 3 | 3 | 0 | 0 | 2 | 9 | 1 | 0 | 0 | 18 | 8 | 8 | 1 | 0 | 7 | 13 | 10 | 2 | 82 |
| 7:45 PM | 0 | 0 | 1 | 8 | 0 | 0 | 8 | 10 | 0 | 0 | 0 | 18 | 0 | 7 | 0 | 0 | 8 | 12 | 13 | 1 | 85 |
| Hourly Total | 0 | 1 | 10 | 22 | 1 | 0 | 29 | 41 | 1 | 0 | 0 | 66 | 22 | 32 | 5 | 0 | 28 | 59 | 54 | 7 | 365 |
| 8:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| daily total | 0 | 7 | 223 | 276 | 4 | 0 | 355 | 560 | 11 | 1 | 4 | 955 | 236 | 347 | 19 | 6 | 246 | 631 | 775 | 58 | 4632 |
| Cars | 0 | 6 | 218 | 270 | 4 | 0 | 345 | 548 | 11 | 1 | 4 | 929 | 227 | 336 | 19 | 6 | 244 | 607 | 742 | 58 | 4493 |
| Heavy Vehicles | 0 | 1 | 5 | 6 | 0 | 0 | 10 | 12 | 0 | 0 | 0 | 26 | 9 | 11 | 0 | 0 | 2 | 24 | 33 | 0 | 139 |
| Heavy Vehicle \% | 0.00\% | 14.29\% | 2.24\% | 2.17\% | 0.00\% | 0.00\% | 2.82\% | 2.14\% | 0.00\% | 0.00\% | 0.00\% | 2.72\% | 3.81\% | 3.17\% | 0.00\% | 0.00\% | 0.81\% | 3.80\% | 4.26\% | 0.00\% | 3.00\% |

Towners Rd \& Hill and Dale Rd

## Carmel Hamlet NY

Wednesday, September 11, 2019


| Total Vehicles On Leg 999 |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vehicles Entering <br> Intersection <br> 506 |  |  |  |  |  |  |  | Vehicles Exiting <br> Intersection |  |  |
| Southbound |  |  |  |  |  |  |  |  |  |  |
| Cars | 270 | 218 | 6 | 0 | 4 |  |  |  |  |  |
| Heavy | 6 | 5 | 1 | 0 | 0 |  |  |  |  |  |
| Total | 276 | 223 | 7 | 0 | 4 |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |


| Total Vehicles on Leg 3455 | Vehicles Entering Intersection 1658 |  | Cars | Heavy | Total |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 58 | 0 | 58 |
|  |  |  | 6 | 0 | 6 |
|  | $\begin{array}{\|c} \text { Vehicles } \\ \text { Exiting } \\ \text { Intersection } \\ 1797 \end{array}$ |  | 244 | 2 | 246 |
|  |  |  | 607 | 24 | 631 |
|  |  |  | 742 | 33 | 775 |


| Cars | Heavy | Total | $\begin{aligned} & \sum_{0}^{\circ} \\ & \frac{\otimes}{0} \\ & \frac{0}{\square} \\ & \vdots \end{aligned}$ | VeniclesEnteringIntersection926 | Total Vehicles on Leg 1911 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 11 | 0 | 11 |  |  |  |
| 548 | 12 | 560 |  |  |  |
| 345 | 10 | 355 |  |  |  |
| 0 | 0 | 0 |  | $\begin{gathered} \text { Exiting } \\ \text { Intersection } \end{gathered}$ |  |
| 1 | 0 | 1 |  | 985 |  |


| Cars | 19 | 4 | 929 | 227 | 336 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heavy | 0 | 0 | 26 | 9 | 11 |
| Total | 19 | 4 | 955 | 236 | 347 |
| Northbound |  |  |  |  |  |
| Vehicles Entering <br> Intersection <br> Total Vehicles On Leg 2892 |  |  |  |  |  |
| Vehicles Exiting <br> Intersection |  |  |  |  |  |
| 1357 |  |  |  |  |  |

TRAFFIC SIGNAL WARRANT SUMMARY

| Project: <br> Location: |  | ounty Roundabout Evaluation | Condition: |  | 2019 Existing Condition |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Towners Rd \& Hill and Dale Rd |  | Lanes: |  | : September 11, 2019 |  |  |
|  | Major Street: | Towners Rd |  | 1 | Critical Approach Speed: | 30 | mph |
|  | Minor Street: | Hill and Dale Rd/Lakeshore Dr | Lanes: | 1 |  |  |  |

## Volume Level Criteria

1. Is the critical speed of major street traffic greater than 40 mph ?
2. Is the intersection in a built-up area of an isolated community with population less than 10,000 ?

|  | No |
| :---: | :---: |
|  | No |
| Criteria used: | 100\% |

WARRANT 1 - EIGHT HOUR VEHICULAR VOLUME
Warrant 1 Satisfied: $\qquad$ NO
Warrant 1 is satisfied if EITHER Condition A OR Condition B is $100 \%$ satisfied.
Warrant 1 is also satisfied if BOTH Condition A AND Condition B are satisfied to the $80 \%$ volume level.

|  |  |  | Condition 1A - Minimum Vehicular Volume( X indicates that criteria is met for specified condition) |  |  |  | $\begin{aligned} & \text { Condition 1B - Interuption of Continuous Traffic } \\ & \text { ( } \mathrm{X} \text { indicates that criteria is met for specified condition) } \end{aligned}$ |  |  |  | Total Satisfied Hours (8 required) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 0 | 0 | 0 |  |  |  |  |
| Minimum Volume Criteria: |  |  |  |  |  |  | 500 | 150 | 400 | 120 | 750 | 75 | 600 | 60 | Condition | Condition | 80\% for |
| $\begin{aligned} & \hline \text { Start } \\ & \text { Time } \end{aligned}$ | Major St. Volume ${ }^{1}$ | Minor St. Volume ${ }^{2}$ | $\begin{gathered} \text { Major St. } \\ 100 \% \end{gathered}$ | $\begin{gathered} \text { Minor St. } \\ 100 \% \end{gathered}$ | $\begin{gathered} \hline \text { Major St. } \\ 80 \% \end{gathered}$ | $\begin{gathered} \text { Minor St. } \\ 80 \% \end{gathered}$ | $\begin{gathered} \hline \text { Major St. } \\ 100 \% \end{gathered}$ | $\begin{gathered} \text { Minor St. } \\ 100 \% \end{gathered}$ | $\begin{gathered} \hline \text { Major St. } \\ 80 \% \end{gathered}$ | $\begin{gathered} \text { Minor St. } \\ 80 \% \end{gathered}$ | 1A <br> Satisfied | 1B <br> Satisfied | Both Satisfied |
| 12:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 1:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 2:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 3:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 4:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 5:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 6:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 7:00 AM | 214 | 63 | - | - | - | - | - | - | - | X | - | - | - |
| 8:00 AM | 192 | 90 | - | - | - | - | - | X | - | X | - | - | - |
| 9:00 AM | 176 | 69 | - | - | - | - | - | - | - | X | - | - | - |
| 10:00 AM | 174 | 88 | - | - | - | - | - | X | - | X | - | - | - |
| 11:00 AM | 181 | 97 | - | - | - | - | - | X | - | X | - | - | - |
| 12:00 PM | 198 | 91 | - | - | - | - | - | X | - | X | - | - | - |
| 1:00 PM | 191 | 95 | - | - | - | - | - | X | - | X | - | - | - |
| 2:00 PM | 231 | 164 | - | X | - | X | - | X | - | X | - | - | - |
| 3:00 PM | 205 | 139 | - | - | - | X | - | X | - | X | - | - | - |
| 4:00 PM | 228 | 198 | - | X | - | X | - | X | - | X | - | - | - |
| 5:00 PM | 253 | 217 | - | X | - | X | - | X | - | X | - | - | - |
| 6:00 PM | 247 | 182 | - | X | - | X | - | X | - | X | - | - | - |
| 7:00 PM | 223 | 126 | - | - | - | X | - | X | - | X | - | - | - |
| 8:00 PM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 9:00 PM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 10:00 PM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 11:00 PM |  |  | - | - | - | - | - | - | - | - | - | - | - |

${ }^{1}$ Major Street Volume is the total combined volume of both mainline approaches.
${ }^{2}$ Minor Street volumes is the highest single side street approach volume.

## WARRANT 2 - FOUR HOUR VEHICULAR VOLUME

Warrant is satisfied if four (4) or more hours satisfy the volume requirements depicted on the four hour warranting graph (see page 2).

| Warrant 2 Satisfied: | NO |
| ---: | ---: |
| No. of Points Above Criteria Curve: | 0 |

## WARRANT 3 - PEAK HOUR VEHICULAR VOLUME

Warrant is satisfied if any hour satisfy the volume requirements depicted on the peak hour warranting graph (see page 3), and ALL three of the following requirement are met.

Warrant 3 Satisfied: $\qquad$
No. of Points Above Criteria Curve: $\qquad$

1. Total stopped time delay on Minor Street equals or exceeds 4 VHD (single lane) or 5 VHD (two lanes):
2. Volume on Minor Street equals or exceeds 100 vehicles (single lane) or 150 vehicles (two lanes):
3. Total intersection volume serviced during the hour equals or exceeds 650 veh. (3-leg) or 800 veh. (4-leg or more):
$\qquad$ VHD Max. $\qquad$

Figure 4C-1. Warrant 2, Four-Hour Vehicular Volume


Note: Points on graph represent hourly volumes. Points above the
respective curve satisfy warrant, points below do not satisfy warrant.

Figure 4C-3. Warrant 3, Peak Hour


Note: Points on graph represent hourly volumes. Points above the
respective curve satisfy warrant, points below do not satisfy warrant.

## Accident Location Information System(ALIS)

## Accident Verbal Description

16408_VDR
Date in this report covers the period - 2/29/2016-2/28/2019
Complete Accident data from NYSDMV is only available thru 2/28/2019 12:00:00 AM
Street: TOWNERS RD


Apparent Factors: NOT APPLICABLE, NOT APPLICABLE
County: Putnam Muni: $\operatorname{Kent(T)~Ref.~Marker:~Street:~TOWNERS~RD~}$
AT INTERSECTION WITH HILL AND DALE RD

| 1/21/2017 | Sat 18:12 PM | Persons Killed: 0 | Persons Injured: 0 |
| :--- | :--- | :---: | :--- |

Public Property Damage: OTHER
School Bus Involved: OTHER
Pre-Accd Action: MAKING LEFT TURN
Apparent Factors: FAILURE TO YIELD RIGHT OF WAY, NOT APPLICABLE
County: Putnam Muni: $\operatorname{Kent(T)~Ref.~Marker:~Street:~TOWNERS~RD~}$


Direction of Travel: EAST
Public Property Damage: OTHER
School Bus Involved: OTHER
Pre-Accd Action: STARTING FROM PARKING
Apparent Factors: TURNING IMPROPER, NOT APPLICABLE
Veh ${ }^{2}$

https://alis.dot.ny.gov/SQRA/SQR_Reports/Default.aspx?p2=\&p4=VT_VERBALREPORT_LOCAL\&p6=Accident Verbal Desc...






9: Hill and Dale Rd/Lakeshore Dr \& Towners Rd

|  | $\rightarrow$ |  |  | $\frac{1}{\dagger}$ |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | NBT | SBT |
| Lane Group Flow (vph) | 124 | 118 | 102 | 66 |
| v/c Ratio | 0.15 | 0.14 | 0.28 | 0.15 |
| Control Delay | 3.8 | 6.4 | 9.8 | 6.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 3.8 | 6.4 | 9.8 | 6.9 |
| Queue Length 50th (ft) | 5 | 13 | 10 | 4 |
| Queue Length 95th (ft) | 20 | 29 | 30 | 18 |
| Internal Link Dist (ft) | 501 | 422 | 652 | 539 |
| Turn Bay Length (ft) |  |  |  |  |
| Base Capacity (vph) | 984 | 1038 | 854 | 1030 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.13 | 0.11 | 0.12 | 0.06 |
| Intersection Summary |  |  |  |  |




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | -1 | F |  | Y |  |
| Traffic Vol, veh/h | 23 | 51 | 98 | 0 | 0 | 55 |
| Future Vol, veh/h | 23 | 51 | 98 | 0 | 0 | 55 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | -10 | 0 | - | 0 | - |
| Peak Hour Factor | 83 | 83 | 83 | 83 | 83 | 83 |
| Heavy Vehicles, \% | 14 | 12 | 3 | 0 | 1 | 1 |
| Mvmt Flow | 28 | 61 | 118 | 0 | 0 | 66 |


| Major/Minor M | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 118 | 0 | - | 0 | 235 | 118 |
| Stage 1 | - | - | - - | - | 118 | - |
| Stage 2 | - | - | - - | - | 117 | - |
| Critical Hdwy | 4.24 | - | - - | - | 6.41 | 6.21 |
| Critical Hdwy Stg 1 | - | - | - - | - | 5.41 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.41 | - |
| Follow-up Hdwy | 2.326 | - | - - | - | 3.509 | 3.309 |
| Pot Cap-1 Maneuver | 1399 | - | - | - | 755 | 937 |
| Stage 1 | - | - | - - | - | 910 | - |
| Stage 2 | - | - | - - | - | 911 | - |
| Platoon blocked, \% |  | - | - - | - |  |  |
| Mov Cap-1 Maneuver | 1399 | - | - - | - | 739 | 937 |
| Mov Cap-2 Maneuver | - | - | - - | - | 739 | - |
| Stage 1 | - | - | - - | - | 891 | - |
| Stage 2 | - | - | - - | - | 911 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 2.4 |  | 0 |  | 9.1 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1399 | - | - | - | 937 |
| HCM Lane V/C Ratio |  | 0.02 |  | - | - | 0.071 |
| HCM Control Delay (s) |  | 7.6 | 0 | - | - | 9.1 |
| HCM Lane LOS |  | A | A | - | - | A |
| HCM 95th \%tile Q(veh) |  | 0.1 | , | - | - | 0.2 |




9: Hill and Dale Rd/Lakeshore Dr \& Towners Rd

|  | $\rightarrow$ | $\checkmark$ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBT | WBT | NBT | SBT |
| Lane Group Flow (vph) | 201 | 81 | 240 | 55 |
| V/c Ratio | 0.34 | 0.14 | 0.57 | 0.12 |
| Control Delay | 7.8 | 8.6 | 14.6 | 5.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 7.8 | 8.6 | 14.6 | 5.8 |
| Queue Length 50th (ft) | 15 | 9 | 32 | 3 |
| Queue Length 95th (ft) | 58 | 33 | 77 | 17 |
| Internal Link Dist (tt) | 501 | 422 | 652 | 539 |
| Turn Bay Length (ft) |  |  |  |  |
| Base Capacity (vph) | 866 | 868 | 828 | 901 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.23 | 0.09 | 0.29 | 0.06 |
| Intersection Summary |  |  |  |  |




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.8 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\mathbf{T}$ |  | Mr |  |
| Traffic Vol, veh/h | 67 | 138 | 72 | 4 | 0 | 51 |
| Future Vol, veh/h | 67 | 138 | 72 | 4 | 0 | 51 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, $\#$ | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | -10 | 0 | - | 0 | - |
| Peak Hour Factor | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, \% | 1 | 1 | 1 | 1 | 1 | 1 |
| Mvmt Flow | 72 | 148 | 77 | 4 | 0 | 55 |


| Major/Minor M | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 81 | 0 | - | 0 | 371 | 79 |
| Stage 1 | - | - | - - | - | 79 | - |
| Stage 2 | - | - | - - | - | 292 | - |
| Critical Hdwy | 4.11 | - |  | - | 6.41 | 6.21 |
| Critical Hdwy Stg 1 | - | - | - - | - | 5.41 | - |
| Critical Hdwy Stg 2 | - | - | - - | - | 5.41 | - |
| Follow-up Hdwy | 2.209 | - | - - | - | 3.509 | 3.309 |
| Pot Cap-1 Maneuver | 1523 | - | - - | - | 632 | 984 |
| Stage 1 | - | - | - - | - | 947 | - |
| Stage 2 | - | - | - - | - | 760 | - |
| Platoon blocked, \% |  | - | - - | - |  |  |
| Mov Cap-1 Maneuver | 1523 | - | - - | - | 599 | 984 |
| Mov Cap-2 Maneuver | - | - | - - | - | 599 | - |
| Stage 1 | - | - | - - | - | 898 | - |
| Stage 2 | - | - | - - | - | 760 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 2.4 |  | 0 |  | 8.9 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 1523 | - | - | - | 984 |
| HCM Lane V/C Ratio |  | 0.047 | - | - | - | 0.056 |
| HCM Control Delay (s) |  | 7.5 | 0 | - | - | 8.9 |
| HCM Lane LOS |  | A | A | - | - | A |
| HCM 95th \%tile Q(veh) |  | 0.1 | A | - | - | 0.2 |

Engineering and Construction Services

ALTERNATE COMMERCIAL PARKING WITH NO GEOMETRIC IMPROVEMENTS

| DESCRIPTION | TOTAL QUANTITY | UNIT | UNIT PRICE | TOTAL COST |
| :---: | :---: | :---: | :---: | :---: |
| PARKING LOTS ${ }^{1}$ | 8,000 | SF | \$12 | \$100,000 |
| ADDITIONAL EARTHWORK (ABOVE AND BEYOND TYPICAL) | 5,000 | CY | \$20 | \$100,000 |
| RETAINING WALL | 950 | SF | \$100 | \$95,000 |
| UTILITY RELOCATION ${ }^{2}$ | 0 | EA | \$75,000 | \$0 |
| STORMWATER AND TREATMENT ${ }^{3}$ | 1 | LS | \$75,000 | \$75,000 |
| WORK ZONE TRAFFIC CONTROL | 1 | LS | \$75,000 | \$75,000 |
|  | ESTIMATED CONSTRUCTION COST (CONCEPTUAL) |  |  | \$445,000 |
| PROPERTY OWNER COORDINATION | 2 | EA | \$75,000 | \$150,000 |
| CONTIGENCY (20\%) | 1 | LS | \$89,000 | \$90,000 |
| DESIGN AND INSPECTION (25\%) | 1 | LS | \$111,250 | \$115,000 |
|  |  |  | FINAL TOTAL | \$800,000 |

${ }^{1}$ INCLUDES TYPICAL COST FOR PAVEMENT, CURB, EARTHWORK, DRAINAGE, LANDSCAPING, ETC., FOR A COMMERICAL PARKING LOT.
${ }^{2}$ ELECTRIC AND GAS RELOCATIONS ARE ASSUMED NO COST FOR MUNICIPAL PROJECTS. WATER AND SEWER RELOCATIONS ARE NOT PRESENT.
${ }^{3}$ IMPACTS OVER 5,000 SF WITHIN DEP WATERSHEDS REQUIRE POST STORMWATER TREATMENT. \$75,000 ALLOWANCE FOR EXTRA ROW OR WORK REQUIRED.

INTERSECTION REALIGNMENT

| DESCRIPTION | TOTAL QUANTITY | UNIT | UNIT PRICE | TOTAL COST |
| :---: | :---: | :---: | :---: | :---: |
| FOUR-WAY INTERSECTION ${ }^{4}$ | 1 | EA | \$300,000 | \$300,000 |
| PARKING LOTS ${ }^{5}$ | 4,000 | SF | \$12 | \$50,000 |
| ADDITONAL EARTHWORK (ABOVE AND BEYOND TYPICAL) | 10,000 | CY | \$20 | \$200,000 |
| RETAINING WALL | 950 | SF | \$100 | \$95,000 |
| UTILITY RELOCATION ${ }^{6}$ | 0 | EA | \$75,000 | \$0 |
| STORMWATER AND TREATMENT ${ }^{7}$ | 1 | LS | \$175,000 | \$175,000 |
| WORK ZONE TRAFFIC CONTROL | 1 | LS | \$150,000 | \$150,000 |
|  | ESTIMATED CONSTRUCTION COST (CONCEPTUAL) |  |  | \$970,000 |
| RIGHT OF WAY (RESIDENTIAL) | 1 | LS | \$8,000 | \$8,000 |
| RIGHT OF WAY (COMMERCIAL) | 0.020 | ACRE | \$340,000 | \$10,000 |
| PROPERTY OWNER COORDINATION | 2 | EA | \$75,000 | \$150,000 |
| CONTIGENCY (20\%) | 1 | LS | \$194,000 | \$195,000 |
| DESIGN AND INSPECTION (25\%) | 1 | LS | \$242,500 | \$245,000 |
|  |  |  | FINAL TOTAL | \$1,580,000 |

[^0]SINGLE LANE ROUNDABOUT (120 FT DIAMETER)

| DESCRIPTION | TOTAL QUANTITY | UNIT | UNIT PRICE | TOTAL COST |
| :---: | :---: | :---: | :---: | :---: |
| SINGLE LANE ROUNDABOUT ${ }^{8}$ | 1 | EA | \$750,000 | \$750,000 |
| THREE-WAY INTERSECTION ${ }^{9}$ | 1 | EA | \$250,000 | \$250,000 |
| ADDITONAL EARTHWORK (ABOVE AND BEYOND TYPICAL) | 10,000 | CY | \$20 | \$200,000 |
| UTILITY RELOCATION ${ }^{10}$ | 0 | EA | \$75,000 | \$0 |
| STORMWATER AND TREATMENT ${ }^{11}$ | 1 | LS | \$175,000 | \$175,000 |
| WORK ZONE TRAFFIC CONTROL | 1 | LS | \$200,000 | \$200,000 |
|  | ESTIMATED CONSTRUCTION COST (CONCEPTUAL) |  |  | \$1,575,000 |
| RIGHT OF WAY (RESIDENTIAL) | 1 | LS | \$8,000 | \$8,000 |
| RIGHT OF WAY (COMMERCIAL) | 1 | LS | \$320,000 | \$320,000 |
| RIGHT OF WAY (COMMERCIAL) | 1 | LS | \$335,000 | \$335,000 |
| CONTIGENCY (20\%) | 1 | LS | \$315,000 | \$315,000 |
| DESIGN AND INSPECTION (25\%) | 1 | LS | \$393,750 | \$395,000 |
|  |  |  | FINAL TOTAL | \$2,950,000 |

8 INCLUDES TYPICAL COST FOR PAVEMENT, CURB, EARTHWORK, DRAINAGE, LANDSCAPING, ETC., FOR A SINGLE LANE ROUNDABOUT.
${ }^{9}$ INCLUDES TYPICAL COST FOR PAVEMENT, CURB, EARTHWORK, DRAINAGE, LANDSCAPING, ETC., FOR A THREE WAY INTERSECTION.
${ }^{10}$ ELECTRIC AND GAS RELOCATIONS ARE ASSUMED NO COST FOR MUNICIPAL PROJECTS. WATER AND SEWER RELOCATIONS ARE NOT PRESENT.
${ }^{11}$ IMPACTS OVER 5,000 SF WITHIN DEP WATERSHEDS REQUIRE POST STORMWATER TREATMENT. \$175,000 ALLOWANCE FOR EXTRA ROW OR WORK REQUIRED.




## SUMMARY OF INTERSECTION EVALUATION FAIRFIELD DR AND HAVILAND DR

## Existing Conditions:

Fairfield Drive in the area of this intersection is a curved road approaching from the west and southeast. Haviland Drive approaches from the northeast. Each of these roadways has a 30 mph speed limit. There is a skew to the intersection and a right turn slip ramp heading northwest, which forms a triangular island between Fairfield Dr, Haviland Dr, and the slip ramp. There is a war memorial in this island, which is inaccessible to pedestrians, as there are no sidewalks or pedestrian crossing facilities at this intersection. Traffic is controlled through the use of an all-way stop condition at the intersection. There is a firehouse in the northwest quadrant of the intersection, and parking for the businesses south of the intersection are accessed through a wide curb cut and parking along the building frontages that requires vehicles to back out into traffic to exit.

Existing capacity and level of service are within an acceptable range, with overall level of service being LOS B during the AM peak and LOS C during the PM peak. The eastbound approach operates at LOS D with a volume to capacity ratio of 0.86 in the PM peak, but that is the only approach that approaches capacity. Though no capacity issues exist, the eastbound queue does extent back approximately 250 feet, and may extend past the midblock pedestrian crossing located west of the intersection. Additionally, the eastbound queue does block parked vehicles in front of the south side businesses from existing their parking spaces, which pose a safety concern. An Intersection Evaluation worksheet, showing geometric details, the existing traffic volumes, and a summary of the capacity analyses is attached.

## Signal Warrant Analysis:

A review of the hourly traffic volumes between 7:00 AM and 8:00 PM show that none of the warrants reviewed; Warrant 1 (8-hour warrant), Warrant 2 (4-hour warrant) or Warrant 3 (peak hour warrant) are satisfied for the existing traffic volumes. Warrant 1 is satisfied for 4 hours and warrant 2 is satisfied for 3 hours, but neither reach the threshold necessary to justify a traffic signal or roundabout. Additionally, fewer than 5 accidents per year occur at this location, so Warrant 7 (Crash Experience) is not satisfied either. See the signal warrant analysis worksheets attached.

## Accident Analysis:

For the 3-year period studied (2016-2018), 7 accidents were reported at this intersection, they range from right angle and left turn to right turn and fixed object, and none resulting in an injury. Overall the accident rate for this location was calculated to be 0.77 accidents/Million Entering Vehicles (MEV), which is 4 times the statewide average for similar intersection on State Roads, but there is no noticeable pattern that reveals a particular concern. However, the existing roadside parking condition that requires vehicles to back out into the travel lane to exit does cause unexpected conflicts that could potential be hazardous and may contribute to the high accident rate at this location. The accidents types and severity are summarized in the table below, and accident records are attached.

ACCIDENT SUMMARY

| Accident Type | Number of Occurrences | Accident Severity | Number of Occurrences |
| :--- | :---: | :--- | :---: |
| Right Angle | 1 | Fatality | 0 |
| Left Turn | 2 | Personal Injury | 0 |
| Rear End | 1 | Property Damage Only | 5 |
| Fixed Object | 2 | Non-Reportable | 2 |
| Right Turn | 1 |  | 7 |
|  | 7 |  |  |

## Field Condition and Right of Way Review:

Right of way is tight in the area and if a roundabout were to be constructed it would require full acquisition of two properties, the demolition of two buildings, and removal of some of the southside store frontage parking. It would also require the relocation of the war memorial, possibly to the center of the roundabout. In addition, the roundabout would require some utility relocations and would need to tie into a significant slope along Haviland Dr.

## Design Alternative Consideration:

Neither a traffic signal or roundabout is warranted here and though a traffic signal would improve the already acceptable levels of service (from $B$ to $A$ in the $A M$ and $C$ to $B$ in the $P M$ ), it could potentially lengthen the already problematic eastbound queue to 400 feet long, which may cause additional blockage time for the adjacent roadside parking and the mid-block crosswalk located approximately 220 feet from the intersection. A roundabout would operate at LOS A in both peaks with much shorter queues, but as mentioned above, would require the acquisition of significant property (see Figure 10 for roundabout footprint and impacts).

To improve operations and safety at the intersection, two main concerns need to be addressed, the excessive eastbound queue resulting from the high number of left turn vehicles on that approach, and the adjacent roadside parking on the south side of the road, which results in traffic backing out into the roadway. Other potential issues, though to a lesser degree, is the entering skew of the southbound, Haviland Dr, approach and the war memorial within the intersection, which does partially block sight distance.

Traffic operations could be improved with the existing intersection geometry by changing traffic control to a stop sign on the side street (Haviland Dr) only. If this were done, level of service would be LOS A for all hours of the day and the longest queue would be approximately 55 feet. However, this would only address the queueing issue, and not the other issues identified.

Two concepts were developed to best address the issues identified. Concept A, which includes an eastbound left turn lane, while maintaining the existing intersection geometry for the other approaches, and Concept B, which adds an eastbound left turn lane, realigns the southbound approach and relocates the war memorial to a location more accessible by pedestrians (see Figures 10A \& 10B for concept sketches for each of these alternatives). In both cases, the left turn lanes can be formed within the County right-of-way, but at the cost of the adjacent roadside parking. As
the commercial developments served by that parking also have a parking lot behind the building, this may not be an issue, but this parking loss should be coordinated with the property owners prior to design. The benefit of removing this parking, in addition to being able to add the left turn lane, is improved safety, as parked vehicles will no longer be backing out into the roadway.

Both Concept A and Concept B can be constructed with an all-way stop condition, same as existing, or with just a side street stop sign and uncontrolled Fairfield Dr approaches. The all-way stop condition is more appropriate for Concept A, as the intersection skew and sight distance limitations from the war memorial will still exist under this concept. With an all-way stop, Concept A should see LOS B overall operations for both peak hours and the maximum eastbound queue should not exceed 75 feet. For Concept $B$, with the skew removed and sight distance improved, it would be reasonable to go to stop sign control on the side street (Haviland Dr) only. If this were done, the level of service would be LOS A overall during both peak hours and the eastbound queues shouldn't exceed one vehicle per lane.

## Conceptual Cost Estimate:

As mentioned above, neither a traffic signal nor roundabout would be an appropriate solution for this location. However, if they were to be constructed, it is estimated that they would cost $\$ 250,000$ and $\$ 2.5 \mathrm{M}$ respectively.

Of the reasonable options available, the cost of removing the stop signs and stop bars on Fairfield Dr to improve the eastbound queuing condition would be minimal. The cost of concept A, with the left turn lane added, would be approximately $\$ 330,000$, and the cost of Concept B, with left turn lane and realigned Haviland Dr would be approximately $\$ 1,280,000$.

These costs are based on our past experience with similar projects, knowledge of construction pricing in this region of New York State and our understanding of the issues. These costs include construction of all improvements, right of way, wetland mitigation, and costs for design and inspection. Cost estimates with a breakdown of the big picture cost items is attached.

## Summary \& Conclusion:

To address all potential issues at this location, Concept B would be the recommended option. However, Concept A is an acceptable alternative that address most of the issues at a much cheaper cost. In both cases, improved safety and reduced eastbound queuing are achieved by adding an eastbound left turn lane and removing the roadside parking near the intersection. If removal of the parking becomes an issue, traffic operations and queuing can be improved by removing the stop signs on Fairfield Dr, but the removal of the stop conditions could increase speeds through the intersection and with the adjacent parking could pose a safety concern. It is understandable that the businesses would want to maximize parking availability and convenience for their customers, but the presence of that roadside parking does yield a less safe condition.


| INTERSECTION EVALUATION WORKSHEET |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | n/a |  |  | Haviland Dr |  |  | Fairfield Dr |  |  | Fairfield Dr |  |  |
|  | Northbound (NE) |  |  | Southbound (SW) |  |  | Eastbound (SE) |  |  | Westbound (NW) |  |  |
|  | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| ANALYSIS SCENARIO \#1 - LEVEL OF SERVICE |  |  |  |  |  |  |  |  |  |  |  |  |
| Description of Improvements: |  |  |  |  |  |  |  |  |  |  |  |  |
| AM Peak Delay (s): |  |  |  |  | 12.8 |  | 8.1 |  |  |  |  |  |
| LOS: |  |  |  |  | B |  | A |  |  |  |  |  |
| $\mathrm{v} / \mathrm{c}$ : |  |  |  |  | 0.44 |  | 0.06 |  |  |  |  |  |
| 95\% Queue: |  |  |  |  | 55' |  | <25' |  |  |  |  |  |
| A (6.4) Overall |  | - |  |  | B (12.8) |  |  | A (3.5) |  |  | A (0.0) |  |
| PM Peak Delay (s): |  |  |  |  | 8.6 |  | 8.2 |  |  |  |  |  |
| LOS: |  |  |  |  | A |  | A |  |  |  |  |  |
| $\mathrm{v} / \mathrm{c}$ : |  |  |  |  | 0.17 |  | 0.23 |  |  |  |  |  |
| 95\% Queue: |  |  |  |  | <25' |  | < $25^{\prime}$ |  |  |  |  |  |
| A (4.5) Overall |  | - |  |  | A (8.6) |  |  | A (4.3) |  |  | A (0.0) |  |
| Note: LOS calculated using HCM 6 methodologies. For unsignalized intersections, only side street approach delay and mainline left turn delay is shown. The HCM 6 methodology assumes zero delay for all other movements. |  |  |  |  |  |  |  |  |  |  |  |  |
| ANALYSIS SCENARIO \#2 - LEVEL OF SERVICE |  |  |  |  |  |  |  |  |  |  |  |  |
| Description of Improvements: Added Eastbound Left Turn Lane with All-Way Sto |  |  |  |  |  |  |  |  |  |  |  |  |
| AM Peak Delay (s): |  |  |  |  | 11.3 |  | 10.2 |  |  |  | 11.4 |  |
| LOS: |  |  |  |  | B |  | B |  |  |  | B |  |
| $\mathrm{v} / \mathrm{c}$ : |  |  |  |  | 0.45 |  | 0.14 |  |  |  | 0.38 |  |
| 95\% Queue: |  |  |  |  | 60' |  | <25' |  |  |  | 45' |  |
| B (11.0) Overall |  | - |  |  | B (11.3) |  |  | A (10.0) |  |  | 3 (11.4) |  |
| PM Peak Delay (s): |  |  |  |  | 10.2 |  | 14.5 |  |  |  | 9.7 |  |
| LOS: |  |  |  |  | B |  | B |  |  |  | A |  |
| $\mathrm{v} / \mathrm{c}$ : |  |  |  |  | 0.28 |  | 0.53 |  |  |  | 0.23 |  |
| 95\% Queue: |  |  |  |  | 30' |  | 75' |  |  |  | <25' |  |
| B (12.1) Overall |  | - |  |  | B (10.2) |  |  | (13.3 |  |  | A (9.7) |  |
| Note: LOS calculated using HCM 6 methodologies. |  |  |  |  |  |  |  |  |  |  |  |  |
| ANALYSIS SCENARIO \#3 - LEVEL OF SERVICE |  |  |  |  |  |  |  |  |  |  |  |  |
| Description of Improvements: Added Eastbound Left Turn Lane with Stop Control on Haviland Dr Only |  |  |  |  |  |  |  |  |  |  |  |  |
| AM Peak Delay (s): |  |  |  |  | 12.8 |  | 8.1 |  |  |  |  |  |
| LOS: |  |  |  |  | B |  | A |  |  |  |  |  |
| $\mathrm{v} / \mathrm{c}$ : |  |  |  |  | 0.43 |  | 0.06 |  |  |  |  |  |
| 95\% Queue: |  |  |  |  | 55' |  | <25' |  |  |  |  |  |
| A (6.4) Overall |  | - |  |  | B (12.9) |  |  | A (3.5) |  |  | A (0.0) |  |
| PM Peak Delay (s): |  |  |  |  | 8.6 |  | 8.2 |  |  |  |  |  |
| LOS: |  |  |  |  | A |  | A |  |  |  |  |  |
| $\mathrm{v} / \mathrm{c}$ : |  |  |  |  | 0.17 |  | 0.23 |  |  |  |  |  |
| 95\% Queue: |  |  |  |  | <25' |  | < 25' |  |  |  |  |  |
| A (4.5) Overall |  | - |  |  | B (8.6) |  |  | A (4.3) |  |  | A (0.0) |  |
| Note: LOS calculated using HCM 6 methodologies. For unsignalized intersections, only side street approach delay and mainline left turn delay is shown. The HCM 6 methodology assumes zero delay for all other movements. |  |  |  |  |  |  |  |  |  |  |  |  |


| INTERSECTION EVALUATION WORKSHEET |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ANALYSIS SCENARIO \#4 - LEVEL OF SERVICE |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Driveway |  |  | Haviland Dr |  |  | Fairfield Dr |  |  | Fairfield Dr |  |  |
|  | Northbound (NE) |  |  | Southbound (SW) |  |  | Eastbound (SE) |  |  | Westbound (NW) |  |  |
|  | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Description of Improvements: Actuated Traffic Signal with No Geometric Improvements |  |  |  |  |  |  |  |  |  |  |  |  |
| AM Peak Delay (s): |  |  |  |  | 12.3 |  |  | 6.6 |  |  |  |  |
| LOS: |  |  |  |  | B |  |  | A |  |  |  |  |
| $\mathrm{v} / \mathrm{c}$ : |  |  |  |  | 0.65 |  |  | 0.28 |  |  |  |  |
| 95\% Queue: |  |  |  |  | 50' |  |  | 65' |  |  |  |  |
| A (9.3) Overall |  | - |  |  | B (12.3) |  |  | A (6.6) |  |  | B (6.9) |  |
| PM Peak Delay (s): |  |  |  |  | 15.3 |  |  | 9.5 |  |  |  |  |
| LOS: |  |  |  |  | B |  |  | A |  |  |  |  |
| v/c: |  |  |  |  | 0.47 |  |  | 0.73 |  |  |  |  |
| 95\% Queue: |  |  |  |  | 60' |  |  | >400' |  |  |  |  |
| B (10.0) Overall |  | - |  |  | B (15.3) |  |  | A (9.5) |  |  | A (4.7) |  |
| Note: LOS calculated using HCM 6 methodologies. Unsignalized delay for westbound right turn is excluded from calculations of the approach delay and intersection delay. |  |  |  |  |  |  |  |  |  |  |  |  |
| ANALYSIS SCENARIO \#5 - LEVEL OF SERVICE |  |  |  |  |  |  |  |  |  |  |  |  |
| Description of Improvements: Single Lane Roundabout - 4 Leg (120' Radius) |  |  |  |  |  |  |  |  |  |  |  |  |
| AM Peak Delay (s): | 3.5 |  |  | 7.2 |  |  | 4.5 |  |  | 4.9 |  |  |
| LOS: | A |  |  | A |  |  | A |  |  | A |  |  |
| v/c: | 0.01 |  |  | 0.35 |  |  | 0.16 |  |  | 0.2 |  |  |
| 95\% Queue: | <25' |  |  | 50' |  |  | $25^{\prime}$ |  |  | $25^{\prime}$ |  |  |
| A (5.8) Overall | A (3.5) |  |  | A (7.2) |  |  | A (4.5) |  |  | A (4.9) |  |  |
| PM Peak Delay (s): | 5.5 |  |  | 4.6 |  |  | 7.9 |  |  | 5.4 |  |  |
| LOS: | A |  |  | A |  |  | A |  |  | A |  |  |
| v/c: | 0.02 |  |  | 0.17 |  |  | 0.49 |  |  | 0.17 |  |  |
| 95\% Queue: | <25' |  |  | $25^{\prime}$ |  |  | 75' |  |  | 25' |  |  |
| A (6.8) Overall | A (5.5) |  |  | A (4.6) |  |  | A (7.9) |  |  | A (5.4) |  |  |

Fairfield Dr \& Haviland Dr
Patterson NY
Wednesday, September 11, 2019

|  |  |  | Southbound Haviland Dr |  |  |  |  | Westbound Fairfield Dr |  |  |  |  | Northbound n/a |  |  |  |  | Eastbound <br> Fairfield Dr |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | U Turns | Left Turns | Through | Turns | Bicycles | U Turns | Left Turns | Through | Turns | Bicycles | U Turns | Left Turns | Through | Turns | Bicycles | U Turns | Left Turns | Through | Turns | Bicycles |  |
| 12:00 AM | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |
| 12:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:00 AM | 0 | 5 | 0 | 86 | 0 | 0 | 0 | 43 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 11 | 0 | 0 | 160 |
| 7:15 AM | 0 | 5 | 0 | 72 | 0 | 0 | 0 | 56 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20 | 17 | 0 | 0 | 171 |
| 7:30 AM | 0 | 9 | 0 | 78 | 0 | 0 | 0 | 60 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 24 | 0 | 0 | 191 |
| 7:45 AM | 0 | 9 | 0 | 67 | 0 | 0 | 1 | 68 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 19 | 0 | 0 | 179 |
| Hourly Total | 0 | 28 | 0 | 303 | 0 | 0 | 1 | 227 | 11 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 60 | 71 | 0 | 0 | 701 |

Fairfield Dr \& Haviland Dr
Patterson NY
Wednesday, September 11, 2019

|  |  |  | Southbound Haviland Dr Straight | Right | Peds/ |  |  | Westbound Fairfield Dr Straight |  | Peds/ |  |  | Northbound n/a Straight | Right | Peds/ |  |  | Eastbound <br> Fairfield Dr Straight | Right | Peds/ | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | U Turns | Left Turns | Through | Turns | Bicycles | U Turns | Left Turns | Through | Turns | Bicycles | U Turns | Left Turns | Through | Turns | Bicycles | U Turns | Left Turns | Through | Turns | Bicycles |  |
| 8:00 AM | 0 | 11 | , | 68 | 0 | 0 | 0 | 48 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 22 | 32 | 0 | 0 | 182 |
| 8:15 AM | 0 | 6 | 0 | 60 | 0 | 0 | 0 | 51 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 25 | 0 | 0 | 162 |
| 8:30 AM | 0 | 12 | 1 | 53 | 0 | 0 | 0 | 55 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 27 | 0 | 0 | 161 |
| 8:45 AM | 0 | 4 | 0 | 32 | 0 | 0 | 1 | 41 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 18 | 0 | 0 | 119 |
| Hourly Total | 0 | 33 | 1 | 213 | 0 | 0 | 1 | 195 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 68 | 102 | 0 | 0 | 624 |
| 9:00 AM | 0 | 4 | 0 | 37 | 0 | 0 | 0 | 37 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 22 | 0 | 0 | 121 |
| 9:15 AM | 0 | 1 | 0 | 47 | 0 | 0 | 0 | 25 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 27 | 0 | 0 | 128 |
| 9:30 AM | 0 | 8 | 0 | 37 | 0 | 0 | 0 | 27 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 18 | 0 | 0 | 119 |
| 9:45 AM | 0 | 5 | 1 | 39 | 0 | 0 | 0 | 30 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 22 | 29 | 0 | 0 | 131 |
| Hourly Total | 0 | 18 | 1 | 160 | 0 | 0 | 0 | 119 | 24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 81 | 96 | 0 | 0 | 499 |
| 10:00 AM | 0 | 2 | 0 | 28 | 1 | 0 | 0 | 26 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 23 | 0 | 0 | 98 |
| 10:15 AM | 0 | 6 | 0 | 40 | 2 | 0 | 0 | 25 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 21 | 0 | 0 | 121 |
| 10:30 AM | 0 | 5 | 0 | 41 | 1 | 0 | 0 | 25 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 29 | 19 | 0 | 0 | 125 |
| 10:45 AM | 0 | 6 | 0 | 26 | 0 | 0 | 0 | 17 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 22 | 26 | 0 | 0 | 101 |
| Hourly Total | 0 | 19 | 0 | 135 | 4 | 0 | 0 | 93 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 90 | 89 | 0 | 0 | 445 |
| 11:00 AM | 0 | 5 | 0 | 33 | 0 | 0 | 0 | 23 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 30 | 14 | 0 | 0 | 114 |
| 11:15 AM | 0 | 2 | 0 | 27 | 0 | 0 | 0 | 23 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 24 | 0 | 1 | 100 |
| 11:30 AM | 0 | 5 | 0 | 34 | 1 | 0 | 0 | 25 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 25 | 24 | 0 | 0 | 125 |
| 11:45 AM | 0 | 7 | 0 | 24 | 0 | 0 | 0 | 18 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 22 | 20 | 0 | 0 | 97 |
| Hourly Total | 0 | 19 | 0 | 118 | 1 | 0 | 0 | 89 | 27 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 100 | 82 | 0 | 1 | 436 |
| 12:00 PM | 0 | 5 | 0 | 31 | 0 | 0 | 0 | 13 | 9 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 31 | 24 | 0 | 2 | 114 |
| 12:15 PM | 0 | 6 | 0 | 30 | 1 | 0 | 1 | 27 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 26 | 20 | 0 | 0 | 113 |
| 12:30 PM | 0 | 7 | 1 | 31 | 0 | 0 | 0 | 19 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 28 | 21 | 0 | 0 | 112 |
| 12:45 PM | 0 | 7 | 0 | 40 | 0 | 0 | 1 | 28 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 26 | 25 | 0 | 0 | 134 |
| Hourly Total | 0 | 25 | 1 | 132 | 1 | 0 | 2 | 87 | 24 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 111 | 90 | 0 | 2 | 473 |
| 1:00 PM | 0 | 2 | 1 | 29 | 0 | 0 | 0 | 24 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 30 | 29 | 0 | 0 | 119 |
| 1:15 PM | 0 | 4 | 0 | 24 | 0 | 0 | 0 | 23 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 27 | 26 | 0 | 1 | 108 |
| 1:30 PM | 0 | 1 | 0 | 29 | 0 | 0 | 0 | 22 | 8 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 31 | 28 | 0 | 1 | 119 |
| 1:45 PM | 0 | 9 | 0 | 31 | 0 | 0 | 0 | 26 | 8 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 20 | 0 | 0 | 118 |
| Hourly Total | 0 | 16 | 1 | 113 | 0 | 0 | 0 | 95 | 24 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 112 | 103 | 0 | 2 | 464 |
| 2:00 PM | 0 | 3 | 0 | 32 | 0 | 0 | 0 | 19 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 36 | 31 | 0 | 0 | 124 |
| 2:15 PM | 0 | 4 | 0 | 37 | 0 | 0 | 0 | 25 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 45 | 37 | 0 | 2 | 155 |
| 2:30 PM | 0 | 5 | 0 | 42 | 0 | 0 | 0 | 21 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 41 | 21 | 0 | 0 | 133 |
| 2:45 PM | 0 | 1 | 0 | 39 | 0 | 0 | 1 | 27 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 37 | 50 | 0 | 0 | 167 |
| Hourly Total | 0 | 13 | 0 | 150 | 0 | 0 | 1 | 92 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 159 | 139 | 0 | 2 | 579 |
| 3:00 PM | 0 | 4 | 0 | 34 | 0 | 0 | 1 | 27 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 42 | 38 | 0 | 0 | 150 |
| 3:15 PM | 0 | 10 | 0 | 32 | 0 | 0 | 0 | 23 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 67 | 42 | 0 | 0 | 181 |
| 3:30 PM | 0 | 4 | 0 | 31 | 0 | 0 | 0 | 44 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 52 | 46 | 0 | 0 | 185 |
| 3:45 PM | 0 | 7 | 0 | 22 | 0 | 0 | 0 | 33 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 77 | 68 | 0 | 1 | 221 |
| Hourly Total | 0 | 25 | 0 | 119 | 0 | 0 | 1 | 127 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 238 | 194 | 0 | 1 | 737 |

Fairfield Dr \& Haviland Dr
Patterson NY
Wednesday, September 11, 2019

|  |  |  | Southbound Haviland Dr Straight | Right | Peds/ |  |  | Westbound Fairfield Dr Straight | Right | Peds/ |  |  | Northbound n/a Straight | Right | Peds/ |  |  | Eastbound <br> Fairfield Dr <br> Straight | Right | Peds/ | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | U Turns | Left Turns | Through | Turns | Bicycles | U Turns | Left Turns | Through | Turns | Bicycles | U Turns | Left Turns | Through | Turns | Bicycles | U Turns | Left Turns | Through | Turns | Bicycles |  |
| 4:00 PM | 0 | 3 | 0 | 35 | 0 | 0 | 0 | 39 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 56 | 60 | 0 | 1 | 196 |
| 4:15 PM | 0 | 4 | 0 | 40 | 0 | 0 | 0 | 27 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 67 | 68 | 0 | 1 | 219 |
| 4:30 PM | 0 | 11 | 0 | 45 | 0 | 0 | 0 | 29 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 75 | 64 | 0 | 1 | 232 |
| 4:45 PM | 0 | 3 | 0 | 40 | 0 | 0 | 1 | 32 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 67 | 68 | 0 | 2 | 217 |
| Hourly Total | 0 | 21 | 0 | 160 | 0 | 0 | 1 | 127 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 265 | 260 | 0 | 5 | 864 |
| 5:00 PM | 0 | 8 | 0 | 35 | 0 | 0 | 0 | 25 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 70 | 65 | 0 | 0 | 214 |
| 5:15 PM | 0 | 5 | 0 | 29 | 0 | 0 | 1 | 35 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 63 | 66 | 0 | 0 | 208 |
| 5:30 PM | 1 | 13 | 0 | 38 | 0 | 0 | 0 | 28 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 72 | 77 | 0 | 0 | 235 |
| 5:45 PM | 0 | 11 | 0 | 41 | 0 | 0 | 0 | 28 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 85 | 57 | 0 | 0 | 226 |
| Hourly Total | 1 | 37 | 0 | 143 | 0 | 0 | 1 | 116 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 290 | 265 | 0 | 0 | 883 |
| 6:00 PM | 0 | 7 | 0 | 34 | 1 | 0 | 0 | 26 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 79 | 72 | 0 | 0 | 226 |
| 6:15 PM | 0 | 8 | 0 | 24 | 0 | 0 | 0 | 28 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 69 | 67 | 0 | 0 | 203 |
| 6:30 PM | 0 | 7 | 0 | 34 | 0 | 0 | 1 | 40 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 53 | 45 | 0 | 0 | 192 |
| 6:45 PM | 0 | 8 | 0 | 35 | 0 | 0 | 0 | 23 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 69 | 53 | 0 | 0 | 195 |
| Hourly Total | 0 | 30 | 0 | 127 | 1 | 0 | 1 | 117 | 34 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 270 | 237 | 0 | 0 | 816 |
| 7:00 PM | 0 | 11 | 0 | 27 | 0 | 1 | 0 | 26 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 43 | 50 | 0 | 1 | 169 |
| 7:15 PM | 0 | 7 | 0 | 25 | 0 | 0 | 0 | 20 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 45 | 44 | 0 | 1 | 154 |
| 7:30 PM | 0 | 5 | 0 | 31 | 0 | 0 | 0 | 22 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 37 | 0 | 0 | 150 |
| 7:45 PM | 0 | 3 | 0 | 18 | 0 | 0 | 0 | 14 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 45 | 34 | 0 | 0 | 124 |
| Hourly Total | 0 | 26 | 0 | 101 | 0 | 1 | 0 | 82 | 45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 177 | 165 | 0 | 2 | 597 |
| 8:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| DAILY TOTAL | 1 | 310 | 4 | 1974 | 7 | 1 | 9 | 1566 | 336 | 3 | 0 | 0 | 0 | 0 | 3 | 3 | 2021 | 1893 | 0 | 15 | 8118 |
| Cars | 1 | 307 | 4 | 1864 | 4 | 1 | 9 | 1513 | 320 | 3 | 0 | 0 | 0 | 0 | 0 | 3 | 1969 | 1786 | 0 | 11 | 7777 |
| Heavy Vehicles | 0 | 3 | 0 | 110 | 3 | 0 | 0 | 53 | 16 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 52 | 107 | 0 | 4 | 341 |
| Heavy Vehicle \% | 0.00\% | 0.97\% | 0.00\% | 5.57\% | 42.86\% | 0.00\% | 0.00\% | 3.38\% | 4.76\% | 0.00\% | 0.00\% | 0.00\% | 0.00\% | 0.00\% | 100.00\% | 0.00\% | 2.57\% | 5.65\% | 0.00\% | 26.67\% | 4.20\% |

Fairfield Dr \& Haviland Dr

## Patterson NY

Wednesday, September 11, 2019


| Total Vehicles On Leg 4647 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Vehicles EnteringIntersection 2289 |  |  | Vehicles ExitingIntersection 2358 |  |  |
| Southbound |  |  |  |  |  |
| Cars | 1864 | 4 | 307 | 1 | 4 |
| Heavy | 110 | 0 | 3 | 0 | 3 |
| Total | 1974 | 4 | 310 | 1 | 7 |


| Total Vehicles on Leg 7460 |  |  | Cars | Heavy | Total |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 11 | 4 | 15 |
|  |  |  | 3 | 0 | 3 |
|  | $\begin{array}{\|c} \text { Vehicles } \\ \text { Exiting } \\ \text { Intersection } \\ 3543 \end{array}$ |  | 1969 | 52 | 2021 |
|  |  |  | 1786 | 107 | 1893 |
|  |  |  | 0 | 0 | 0 |

$\left.\begin{array}{|c|c|c|c|c|c|}\hline \text { Cars } & \text { Heavy } & \text { Total } & & \begin{array}{c}\text { Vehicles }\end{array} \\ \hline & 320 & 16 & \mathbf{3 3 6} & & \begin{array}{c}\text { Entering } \\ \text { Intersection } \\ 1912\end{array} \\ \hline\end{array} \begin{array}{c}\text { Total } \\ \text { Vehicles } \\ \text { on Leg }\end{array}\right)$


## TRAFFIC SIGNAL WARRANT SUMMARY



## Volume Level Criteria

1. Is the critical speed of major street traffic greater than 40 mph ?
2. Is the intersection in a built-up area of an isolated community with population less than 10,000 ?

|  | No |
| ---: | :---: |
| Criteria used: | No |
|  | $100 \%$ |

WARRANT 1 - EIGHT HOUR VEHICULAR VOLUME
Warrant 1 Satisfied: $\qquad$ NO
Warrant 1 is satisfied if EITHER Condition A OR Condition B is $100 \%$ satisfied
Warrant 1 is also satisfied if BOTH Condition A AND Condition B are satisfied to the $80 \%$ volume level.

|  |  |  | Condition 1A - Minimum Vehicular Volume( X indicates that criteria is met for specified condition) |  |  |  | Condition 1B - Interuption of Continuous Traffic ( X indicates that criteria is met for specified condition) |  |  |  | Total Satisfied Hours (8 required) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 4 | 0 | 4 |  |  |  |  |
| Minimum Volume Criteria: |  |  |  |  |  |  | 500 | 150 | 400 | 120 | 750 | 75 | 600 | 60 | Condition | Condition | $80 \% \text { for }$ |
| $\begin{aligned} & \hline \text { Start } \\ & \text { Time } \end{aligned}$ | Major St. Volume ${ }^{1}$ | Minor St. Volume ${ }^{2}$ | Major St. 100\% | Minor St. 100\% | Major St. 80\% | $\begin{aligned} & \text { Minor St. } \\ & 80 \% \end{aligned}$ | $\begin{gathered} \text { Major St. } \\ 100 \% \end{gathered}$ | Minor St. 100\% | Major St. <br> 80\% | $\begin{gathered} \text { Minor St. } \\ 80 \% \end{gathered}$ | $1 \mathrm{~A}$ <br> Satisfied | 1B <br> Satisfied | Both Satisfied |
| 12:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 1:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 2:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 3:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 4:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 5:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 6:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 7:00 AM | 389 | 348 | - | X | - | X | - | X | - | X | - | - | - |
| 8:00 AM | 396 | 259 | - | X | - | X | - | X | - | X | - | - | - |
| 9:00 AM | 336 | 188 | - | X | - | X | - | X | - | X | - | - | - |
| 10:00 AM | 306 | 162 | - | X | - | X | - | X | - | X | - | - | - |
| 11:00 AM | 314 | 144 | - | - | - | X | - | X | - | X | - | - | - |
| 12:00 PM | 331 | 166 | - | X | - | X | - | X | - | X | - | - | - |
| 1:00 PM | 351 | 137 | - | - | - | X | - | X | - | X | - | - | - |
| 2:00 PM | 437 | 171 | - | X | X | X | - | X | - | X | - | - | - |
| 3:00 PM | 623 | 151 | X | X | X | X | - | X | X | X | 1 | - | 1 |
| 4:00 PM | 717 | 190 | X | X | X | X | - | X | X | X | 1 | - | 1 |
| 5:00 PM | 737 | 190 | X | X | X | X | - | X | X | X | 1 | - | 1 |
| 6:00 PM | 692 | 165 | X | X | X | X | - | X | X | X | 1 | - | 1 |
| 7:00 PM | 494 | 133 | - | - | X | X | - | X | - | X | - | - | - |
| 8:00 PM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 9:00 PM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 10:00 PM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 11:00 PM |  |  | - | - | - | - | - | - | - | - | - | - | - |

${ }^{1}$ Major Street Volume is the total combined volume of both mainline approaches
${ }^{2}$ Minor Street volumes is the highest single side street approach volume.
Note: Right turn traffic was removed from side street volume and only one of the two available lanes was considered in the Warrant analysis.

WARRANT 2 - FOUR HOUR VEHICULAR VOLUME
Warrant is satisfied if four (4) or more hours satisfy the volume requirements depicted on the four hour warranting graph (see page 2).

| Warrant 2 Satisfied: | NO |
| ---: | ---: |
| No. of Points Above Criteria Curve: | 3 | 3

$\qquad$ No. of Points Above Criteria Curve: $\qquad$ 0

1. Total stopped time delay on Minor Street equals or exceeds 4 VHD (single lane) or 5 VHD (two lanes):
2. Volume on Minor Street equals or exceeds 100 vehicles (single lane) or 150 vehicles (two lanes):
3. Total intersection volume serviced during the hour equals or exceeds 650 veh. (3-leg) or 800 veh. (4-leg or more):
$\qquad$ VHD Max. $\qquad$

Figure 4C-1. Warrant 2, Four-Hour Vehicular Volume


Note: Points on graph represent hourly volumes. Points above the
respective curve satisfy warrant, points below do not satisfy warrant.

Figure 4C-3. Warrant 3, Peak Hour


Note: Points on graph represent hourly volumes. Points above the
respective curve satisfy warrant, points below do not satisfy warrant.

## Accident Location Information System(ALIS)

## Accident Verbal Description

16408_VDR
Date in this report covers the period - 2/29/2016-2/28/2019
Complete Accident data from NYSDMV is only available thru 2/28/2019 12:00:00 AM

 Pre-Accd Action: MAKING RIGHT TURN

Apparent Factors: TURNING IMPROPER, NOT APPLICABLE


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 11.5 |
| Intersection LOS | B |


| Movement | SEL | SET | NWT | NWR | SWL | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ | 4 | 「 | * |  |
| Traffic Vol, veh/h | 75 | 97 | 244 | 8 | 36 | 299 |
| Future Vol, veh/h | 75 | 97 | 244 | 8 | 36 | 299 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles, \% | 14 | 14 | 3 | 1 | 1 | 3 |
| Mvmt Flow | 79 | 102 | 257 | 8 | 38 | 315 |
| Number of Lanes | 0 | 1 | 1 | 1 | 1 | 0 |
| Approach | SE |  | NW |  | SW |  |
| Opposing Approach | NW |  | SE |  |  |  |
| Opposing Lanes | 2 |  | 1 |  | 0 |  |
| Conflicting Approach Left | SW |  |  |  | NW |  |
| Conflicting Lanes Left | 1 |  | 0 |  | 2 |  |
| Conflicting Approach Right |  |  | SW |  | SE |  |
| Conflicting Lanes Right | 0 |  | 1 |  | 1 |  |
| HCM Control Delay | 10.9 |  | 12.1 |  | 11.4 |  |
| HCM LOS | B |  | B |  | B |  |


| Lane | NWLn1 | NWLn2 | SELn1 | SWLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $0 \%$ | $44 \%$ | $11 \%$ |
| Vol Thru, \% | $100 \%$ | $0 \%$ | $56 \%$ | $0 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $89 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 244 | 8 | 172 | 335 |
| LT Vol | 0 | 0 | 75 | 36 |
| Through Vol | 244 | 0 | 97 | 0 |
| RT Vol | 0 | 8 | 0 | 299 |
| Lane Flow Rate | 257 | 8 | 181 | 353 |
| Geometry Grp | 7 | 7 | 5 | 2 |
| Degree of Util (X) | 0.405 | 0.012 | 0.283 | 0.449 |
| Departure Headway (Hd) | 5.683 | 4.94 | 5.635 | 4.579 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 637 | 728 | 641 | 776 |
| Service Time | 3.387 | 2.644 | 3.643 | 2.665 |
| HCM Lane V/C Ratio | 0.403 | 0.011 | 0.282 | 0.455 |
| HCM Control Delay | 12.2 | 7.7 | 10.9 | 11.4 |
| HCM Lane LOS | B | A | B | B |
| HCM 95th-tile Q | 2 | 0 | 1.2 | 2.3 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 6.4 |  |  |  |  |  |
| Movement | SEL | SET | NWT | NWR | SWL | SWR |
| Lane Configurations |  | $\mathbf{- 1}$ | $\mathbf{4}$ | $\mathbf{7}$ | Mr |  |
| Traffic Vol, veh/h | 75 | 97 | 244 | 8 | 36 | 299 |
| Future Vol, veh/h | 75 | 97 | 244 | 8 | 36 | 299 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 1 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | Stop | - | None |
| Storage Length | - | - | - | 65 | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | -10 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 14 | 14 | 3 | 1 | 1 | 3 |
| Mvmt Flow | 79 | 102 | 257 | 8 | 38 | 315 |


| Major/Minor | Major1 |  |  |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 257 | 0 |  | 0 | 518 | 257 |
| Stage 1 | - | - |  | - | 257 | - |
| Stage 2 | - | - |  | - | 261 | - |
| Critical Hdwy | 4.24 | - |  | - | 4.41 | 5.23 |
| Critical Hdwy Stg 1 | - | - | - | - | 3.41 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 3.41 | - |
| Follow-up Hdwy | 2.326 | - | - | - | 3.509 | 3.327 |
| Pot Cap-1 Maneuver | 1241 | - | - | - | 693 | 837 |
| Stage 1 | - | - | - | - | 909 | - |
| Stage 2 | - | - | - | - | 907 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1241 | - | - | - | 647 | 837 |
| Mov Cap-2 Maneuver | - | - | - | - | 647 | - |
| Stage 1 | - | - | - | - | 848 | - |
| Stage 2 | - | - | - | - | 907 | - |
|  |  |  |  |  |  |  |
| Approach | SE |  | NW |  | SW |  |
| HCM Control Delay, s | 3.5 |  | 0 |  | 12.8 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NWT NWR |  | SEL | SETSWLn1 |  |
| Capacity (veh/h) |  | - | - | 1241 | - | 811 |
| HCM Lane V/C Ratio |  | - | - | 0.064 | - | 0.435 |
| HCM Control Delay (s) |  | - | - | 8.1 | 0 | 12.8 |
| HCM Lane LOS |  | - | - | A | A | B |
| HCM 95th \%tile Q(veh) |  | - | - | 0.2 | - | 2.2 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 6.4 |  |  |  |  |  |
| Movement | SEL | SET | NWT | NWR | SWL | SWR |
| Lane Configurations | $\mathbf{1}$ | 4 | $\mathbf{4}$ | $\mathbf{7}$ | M |  |
| Traffic Vol, veh/h | 75 | 97 | 244 | 8 | 36 | 299 |
| Future Vol, veh/h | 75 | 97 | 244 | 8 | 36 | 299 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 1 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | Stop | - | None |
| Storage Length | 75 | - | - | 65 | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | -10 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 14 | 14 | 3 | 1 | 1 | 3 |
| Mvmt Flow | 79 | 102 | 257 | 8 | 38 | 315 |


| Major/Minor | Major1 |  |  |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 257 | 0 |  | 0 | 518 | 257 |
| Stage 1 | - | - |  | - | 257 | - |
| Stage 2 | - | - |  | - | 261 | - |
| Critical Hdwy | 4.24 | - |  | - | 4.41 | 5.23 |
| Critical Hdwy Stg 1 | - | - | - | - | 3.41 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 3.41 | - |
| Follow-up Hdwy | 2.326 | - | - | - | 3.509 | 3.327 |
| Pot Cap-1 Maneuver | 1241 | - | - | - | 693 | 837 |
| Stage 1 | - | - | - | - | 909 | - |
| Stage 2 | - | - | - | - | 907 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1241 | - | - | - | 649 | 837 |
| Mov Cap-2 Maneuver | - | - | - | - | 649 | - |
| Stage 1 | - | - | - | - | 851 | - |
| Stage 2 | - | - | - | - | 907 | - |
|  |  |  |  |  |  |  |
| Approach | SE |  | NW |  | SW |  |
| HCM Control Delay, s | 3.5 |  | 0 |  | 12.8 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NWT NWR |  | SEL | SETSWLn1 |  |
| Capacity (veh/h) |  | - | - | 1241 | - | 812 |
| HCM Lane V/C Ratio |  | - | - | 0.064 | - | 0.434 |
| HCM Control Delay (s) |  | - | - | 8.1 | - | 12.8 |
| HCM Lane LOS |  | - | - | A | - | B |
| HCM 95th \%tile Q(veh) |  | - | - | 0.2 | - | 2.2 |


| Intersection |
| :--- |
| Intersection Delay, s/veh |
| Intersection LOS |


| Movement | SEL | SET | NWT | NWR | SWL | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 4 | $\uparrow$ |  | M |  |
| Traffic Vol, veh/h | 75 | 97 | 244 | 8 | 36 | 299 |
| Future Vol, veh/h | 75 | 97 | 244 | 8 | 36 | 299 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles, \% | 14 | 14 | 3 | 1 | 1 | 3 |
| Mvmt Flow | 79 | 102 | 257 | 8 | 38 | 315 |
| Number of Lanes | 1 | 1 | 1 | 0 | 1 | 0 |
| Approach | SE |  | NW |  | SW |  |
| Opposing Approach | NW |  | SE |  |  |  |
| Opposing Lanes | 1 |  | 2 |  | 0 |  |
| Conflicting Approach Left | SW |  |  |  | NW |  |
| Conflicting Lanes Left | 1 |  | 0 |  | 1 |  |
| Conflicting Approach Right |  |  | SW |  | SE |  |
| Conflicting Lanes Right | 0 |  | 1 |  | 2 |  |
| HCM Control Delay | 10 |  | 11.4 |  | 11.3 |  |
| HCM LOS | A |  | B |  | B |  |


| Lane | NWLn1 | SELn1 | SELn2 | SWLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $100 \%$ | $0 \%$ | $11 \%$ |
| Vol Thru, \% | $97 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, \% | $3 \%$ | $0 \%$ | $0 \%$ | $89 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 252 | 75 | 97 | 335 |
| LT Vol | 0 | 75 | 0 | 36 |
| Through Vol | 244 | 0 | 97 | 0 |
| RT Vol | 8 | 0 | 0 | 299 |
| Lane Flow Rate | 265 | 79 | 102 | 353 |
| Geometry Grp | 5 | 7 | 7 | 2 |
| Degree of Util (X) | 0.384 | 0.142 | 0.169 | 0.445 |
| Departure Headway (Hd) | 5.21 | 6.454 | 5.948 | 4.54 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 695 | 558 | 607 | 783 |
| Service Time | 3.21 | 4.161 | 3.655 | 2.623 |
| HCM Lane V/C Ratio | 0.381 | 0.142 | 0.168 | 0.451 |
| HCM Control Delay | 11.4 | 10.2 | 9.9 | 11.3 |
| HCM Lane LOS | B | B | A | B |
| HCM 95th-tile Q | 1.8 | 0.5 | 0.6 | 2.3 |


|  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
|  |  |  |  |  |
|  | SET | NWT | NWR | SWL |
| Lane Group | 181 | 257 | 8 | 353 |
| Lane Group Flow (vph) | 0.42 | 0.42 | 0.01 | 0.54 |
| v/c Ratio | 11.2 | 9.9 | 4.2 | 6.0 |
| Control Delay | 0.0 | 0.0 | 0.0 | 0.0 |
| Queue Delay | 11.2 | 9.9 | 4.2 | 6.0 |
| Total Delay | 22 | 30 | 0 | 5 |
| Queue Length 50th (ft) | 63 | 78 | 5 | 49 |
| Queue Length 95th (ft) | 586 | 723 |  | 611 |
| Internal Link Dist (ft) |  |  | 65 |  |
| Turn Bay Length (ft) | 964 | 1389 | 1328 | 799 |
| Base Capacity (vph) | 0 | 0 | 0 | 0 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0.19 | 0.19 | 0.01 | 0.44 |
| Reduced v/c Ratio |  |  |  |  |
| Intersection Summary |  |  |  |  |



| Intersection Summary |  |
| :--- | ---: |
| HCM 6th Ctrl Delay | 9.3 |
| HCM 6th LOS | A |

## Notes

Unsignalized Delay for [NWR] is excluded from calculations of the approach delay and intersection delay.

| Intersection |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Intersection Delay, s/veh | 5.8 |  |  |  |
| Intersection LOS | A |  | NW | NE |
| Approach | SE | 1 | 1 | SW |
| Entry Lanes | 1 | 1 | 1 | 1 |
| Conflicting Circle Lanes | 1 | 15 | 1 |  |
| Adj Approach Flow, veh/h | 186 | 15 | 358 |  |
| Demand Flow Rate, veh/h | 211 | 270 | 367 |  |
| Vehicles Circulating, veh/h | 48 | 278 | 275 |  |
| Vehicles Exiting, veh/h | 594 | 100 | 15 | 103 |
| Ped Vol Crossing Leg, \#/h | 0 | 159 | 0 |  |
| Ped Cap Adj | 1.00 | 1 | 1.000 | 1.000 |
| Approach Delay, s/veh | 4.5 | 1.000 | 7.2 |  |
| Approach LOS | A | 4.9 | A | A |


| Lane | Left | Left | Left | Left |
| :--- | :---: | ---: | :---: | ---: |
| Designated Moves | LTR | LTR | LTR | LTR |
| Assumed Moves | LTR | LTR | LTR |  |
| RT Channelized |  |  |  |  |
| Lane Util | 1.000 | 1.000 | 1.000 | 1.000 |
| Follow-Up Headway, s | 2.609 | 2.609 | 2.609 | 4.909 |
| Critical Headway, s | 4.976 | 4.976 | 4.976 | 367 |
| Entry Flow, veh/h | 211 | 278 | 15 | 1042 |
| Cap Entry Lane, veh/h | 1314 | 1246 | 1076 | 0.975 |
| Entry HV Adj Factor | 0.880 | 0.972 | 0.997 | 358 |
| Flow Entry, veh/h | 186 | 270 | 15 | 1017 |
| Cap Entry, veh/h | 1157 | 1211 | 1072 | 0.352 |
| V/C Ratio | 0.161 | 0.223 | 7.2 |  |
| Control Delay, s/veh | 4.5 | 4.9 | 3.5 | A |
| LOS | A | 1 | 0 | 2 |


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh | 22.4 |
| Intersection LOS | C |


| Movement | SEL | SET | NWT | NWR | SWL | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\uparrow$ | 4 | 「 | * |  |
| Traffic Vol, veh/h | 314 | 286 | 123 | 28 | 38 | 149 |
| Future Vol, veh/h | 314 | 286 | 123 | 28 | 38 | 149 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles, \% | 1 | 1 | 3 | 1 | 1 | 3 |
| Mvmt Flow | 331 | 301 | 129 | 29 | 40 | 157 |
| Number of Lanes | 0 | 1 | 1 | 1 | 1 | 0 |
| Approach | SE |  | NW |  | SW |  |
| Opposing Approach | NW |  | SE |  |  |  |
| Opposing Lanes | 2 |  | 1 |  | 0 |  |
| Conflicting Approach Left | SW |  |  |  | NW |  |
| Conflicting Lanes Left | 1 |  | 0 |  | 2 |  |
| Conflicting Approach Right |  |  | SW |  | SE |  |
| Conflicting Lanes Right | 0 |  | 1 |  | 1 |  |
| HCM Control Delay | 29.2 |  | 9.6 |  | 10.7 |  |
| HCM LOS | D |  | A |  | B |  |


| Lane | NWLn1 | NWLn2 | SELn1 | SWLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $0 \%$ | $52 \%$ | $20 \%$ |
| Vol Thru, \% | $100 \%$ | $0 \%$ | $48 \%$ | $0 \%$ |
| Vol Right, \% | $0 \%$ | $100 \%$ | $0 \%$ | $80 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 123 | 28 | 600 | 187 |
| LT Vol | 0 | 0 | 314 | 38 |
| Through Vol | 123 | 0 | 286 | 0 |
| RT Vol | 0 | 28 | 0 | 149 |
| Lane Flow Rate | 129 | 29 | 632 | 197 |
| Geometry Grp | 7 | 7 | 5 | 2 |
| Degree of Util (X) | 0.207 | 0.041 | 0.85 | 0.298 |
| Departure Headway (Hd) | 5.769 | 5.025 | 4.847 | 5.446 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 624 | 715 | 739 | 663 |
| Service Time | 3.485 | 2.74 | 2.943 | 3.446 |
| HCM Lane V/C Ratio | 0.207 | 0.041 | 0.855 | 0.297 |
| HCM Control Delay | 10 | 8 | 29.2 | 10.7 |
| HCM Lane LOS | A | A | D | B |
| HCM 95th-tile Q | 0.8 | 0.1 | 9.9 | 1.2 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 4.5 |  |  |  |  |  |
| Movement | SEL | SET | NWT | NWR | SWL | SWR |
| Lane Configurations |  | $\mathbf{- 1}$ | $\mathbf{4}$ | $\mathbf{7}$ | M |  |
| Traffic Vol, veh/h | 314 | 286 | 123 | 28 | 38 | 149 |
| Future Vol, veh/h | 314 | 286 | 123 | 28 | 38 | 149 |
| Conflicting Peds, \#/hr | 1 | 0 | 0 | 1 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Stop | - | Stop | - | Stop |
| Storage Length | - | - | - | 65 | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | -10 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 1 | 1 | 3 | 1 | 1 | 3 |
| Mvmt Flow | 331 | 301 | 129 | 29 | 40 | 157 |



| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 4.5 |  |  |  |  |  |  |
| Movement | SEL | SET | NWT | NWR | SWL | SWR |
| Lane Configurations | ${ }^{*}$ | 4 | 4 | 「 | M |  |
| Traffic Vol, veh/h | 314 | 286 | 123 | 28 | 38 | 149 |
| Future Vol, veh/h | 314 | 286 | 123 | 28 | 38 | 149 |
| Conflicting Peds, \#/hr | 1 | 0 | 0 | 1 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | Stop | - | Stop | - | Stop |
| Storage Length | 75 | - | - | 65 | 0 | - |
| Veh in Median Storage, \# | \# | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | -10 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 1 | 1 | 3 | 1 | 1 | 3 |
| Mvmt Flow | 331 | 301 | 129 | 29 | 40 | 157 |


| Major/Minor M | Major1 |  |  |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 130 | 0 |  | 0 | 1093 | 130 |
| Stage 1 | - | - |  | - | 130 | - |
| Stage 2 | - | - |  | - | 963 | - |
| Critical Hdwy | 4.11 | - |  | - | 4.41 | 5.23 |
| Critical Hdwy Stg 1 | - | - | - | - | 3.41 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 3.41 | - |
| Follow-up Hdwy | 2.209 | - | - | - | 3.509 | 3.327 |
| Pot Cap-1 Maneuver | 1462 | - | - | - | 437 | 951 |
| Stage 1 | - | - | - | - | 966 | - |
| Stage 2 | - | - | - | - | 635 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1461 | - | - | - | 337 | 950 |
| Mov Cap-2 Maneuver | - | - | - | - | 337 | - |
| Stage 1 | - | - | - | - | 746 | - |
| Stage 2 | - | - | - | - | 634 | - |
|  |  |  |  |  |  |  |
| Approach | SE |  | NW |  | SW |  |
| HCM Control Delay, s | 4.3 |  | 0 |  | 8.6 |  |
| HCM LOS |  |  |  |  | A |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NWT NWR SEL SETSWLn1 |  |  |  |  |
| Capacity (veh/h) |  | - | - | - 1461 | - 1192 |  |
| HCM Lane V/C Ratio |  | - | - | - 0.226 | - 0.165 |  |
| HCM Control Delay (s) |  | - | - | 8.2 | - | 8.6 |
| HCM Lane LOS |  | - | - | A | - | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.9 |  | 0.6 |


| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 12.1 |
| Intersection LOS | B |


| Movement | SEL | SET | NWT | NWR | SWL | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | 4 | $\uparrow$ |  | M |  |
| Traffic Vol, veh/h | 314 | 286 | 123 | 28 | 38 | 149 |
| Future Vol, veh/h | 314 | 286 | 123 | 28 | 38 | 149 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles, \% | 1 | 1 | 3 | 1 | 1 | 3 |
| Mvmt Flow | 331 | 301 | 129 | 29 | 40 | 157 |
| Number of Lanes | 1 | 1 | 1 | 0 | 1 | 0 |
| Approach | SE |  | NW |  | SW |  |
| Opposing Approach | NW |  | SE |  |  |  |
| Opposing Lanes | 1 |  | 2 |  | 0 |  |
| Conflicting Approach Left | SW |  |  |  | NW |  |
| Conflicting Lanes Left | 1 |  | 0 |  | 1 |  |
| Conflicting Approach Right |  |  | SW |  | SE |  |
| Conflicting Lanes Right | 0 |  | 1 |  | 2 |  |
| HCM Control Delay | 13.3 |  | 9.7 |  | 10.2 |  |
| HCM LOS | B |  | A |  | B |  |


| Lane | NWLn1 | SELn1 | SELn2 | SWLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Vol Left, \% | $0 \%$ | $100 \%$ | $0 \%$ | $20 \%$ |
| Vol Thru, \% | $81 \%$ | $0 \%$ | $100 \%$ | $0 \%$ |
| Vol Right, \% | $19 \%$ | $0 \%$ | $0 \%$ | $80 \%$ |
| Sign Control | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 151 | 314 | 286 | 187 |
| LT Vol | 0 | 314 | 0 | 38 |
| Through Vol | 123 | 0 | 286 | 0 |
| RT Vol | 28 | 0 | 0 | 149 |
| Lane Flow Rate | 159 | 331 | 301 | 197 |
| Geometry Grp | 5 | 7 | 7 | 2 |
| Degree of Util (X) | 0.225 | 0.521 | 0.432 | 0.281 |
| Departure Headway (Hd) | 5.105 | 5.675 | 5.171 | 5.148 |
| Convergence, Y/N | Yes | Yes | Yes | Yes |
| Cap | 696 | 631 | 692 | 695 |
| Service Time | 3.186 | 3.445 | 2.942 | 3.208 |
| HCM Lane V/C Ratio | 0.228 | 0.525 | 0.435 | 0.283 |
| HCM Control Delay | 9.7 | 14.5 | 11.9 | 10.2 |
| HCM Lane LOS | A | B | B | B |
| HCM 95th-tile Q | 0.9 | 3 | 2.2 | 1.2 |


|  | , | k |  | 5 |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | SET | NWT | NWR | SWL |
| Lane Group Flow (vph) | 632 | 129 | 29 | 197 |
| v/c Ratio | 0.89 | 0.14 | 0.03 | 0.49 |
| Control Delay | 28.6 | 4.8 | 2.0 | 10.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 28.6 | 4.8 | 2.0 | 10.7 |
| Queue Length 50th (ft) | 145 | 14 | 0 | 11 |
| Queue Length 95th (ft) | \#396 | 35 | 7 | 57 |
| Internal Link Dist (ft) | 962 | 723 |  | 611 |
| Turn Bay Length (ft) |  |  | 65 |  |
| Base Capacity (vph) | 709 | 922 | 874 | 502 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.89 | 0.14 | 0.03 | 0.39 |
| Intersection Summary |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longerQueue shown is maximum after two cycles. |  |  |  |  |
|  |  |  |  |  |



## Notes

Unsignalized Delay for [NWR] is excluded from calculations of the approach delay and intersection delay.

| Intersection |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 6.8 |  |  |  |  |  |  |  |
| Intersection LOS | A |  |  |  |  |  |  |  |
| Approach |  | SE |  | NW |  | NE |  | SW |
| Entry Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Conflicting Circle Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Adj Approach Flow, veh/h |  | 637 |  | 163 |  | 15 |  | 202 |
| Demand Flow Rate, veh/h |  | 643 |  | 167 |  | 15 |  | 207 |
| Vehicles Circulating, veh/h |  | 50 |  | 344 |  | 678 |  | 143 |
| Vehicles Exiting, veh/h |  | 300 |  | 349 |  | 15 |  | 368 |
| Ped Vol Crossing Leg, \#/h |  | 0 |  | 1 |  | 0 |  | 0 |
| Ped Cap Adj |  | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |
| Approach Delay, s/veh |  | 7.9 |  | 5.4 |  | 5.5 |  | 4.6 |
| Approach LOS |  | A |  | A |  | A |  | A |
| Lane | Left |  | Left |  | Left |  | Left |  |
| Designated Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| Assumed Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| RT Channelized |  |  |  |  |  |  |  |  |
| Lane Util | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |  |
| Follow-Up Headway, s | 2.609 |  | 2.609 |  | 2.609 |  | 2.609 |  |
| Critical Headway, s | 4.976 |  | 4.976 |  | 4.976 |  | 4.976 |  |
| Entry Flow, veh/h | 643 |  | 167 |  | 15 |  | 207 |  |
| Cap Entry Lane, veh/h | 1311 |  | 972 |  | 691 |  | 1193 |  |
| Entry HV Adj Factor | 0.991 |  | 0.977 |  | 0.997 |  | 0.976 |  |
| Flow Entry, veh/h | 637 |  | 163 |  | 15 |  | 202 |  |
| Cap Entry, veh/h | 1299 |  | 949 |  | 689 |  | 1163 |  |
| V/C Ratio | 0.490 |  | 0.172 |  | 0.022 |  | 0.174 |  |
| Control Delay, s/veh | 7.9 |  | 5.4 |  | 5.5 |  | 4.6 |  |
| LOS | A |  | A |  | A |  | A |  |
| 95th \%tile Queue, veh | 3 |  | 1 |  | 0 |  | 1 |  |

GPI Greenman-Pedersen, Inc.

Engineering and Construction Services

| Intersection: | Fairfield Dr \& Haviland Dr |
| ---: | :--- |
| Client: | Putnam County |
| Calculated By: | D. Creen |
| Checked By: | M. Wieszchowski |

ACTUATED TRAFFIC SIGNAL WITH NO GEOMETRIC IMPROVEMENTS

| DESCRIPTION | TOTAL QUANTITY | UNIT | UNIT PRICE | TOTAL COST |
| :---: | :---: | :---: | :---: | :---: |
| ACTUATED TRAFFIC SIGNAL ${ }^{1}$ | 1 | EA | \$150,000 | \$150,000 |
| WORK ZONE TRAFFIC CONTROL | 1 | LS | \$20,000 | \$20,000 |
|  | ESTIMATED CONSTRUCTION COST (CONCEPTUAL) |  |  | \$170,000 |
| CONTIGENCY (20\%) | 1 | LS | \$34,000 | \$35,000 |
| DESIGN AND INSPECTION (25\%) | 1 | LS | \$42,500 | \$45,000 |
|  |  |  | FINAL TOTAL | \$250,000 |

${ }^{1}$ INCLUDES TYPICAL COST FOR CONTROLLER, SIGNAL POLES, LOOPS, WIRING, SIGNAL HEADS, ETC., FOR AN ACTUATED TRAFFIC SIGNAL.

EASTBOUND LEFT TURN LANE

| DESCRIPTION | TOTAL QUANTITY | UNIT | UNIT PRICE | TOTAL COST |
| :---: | :---: | :---: | :---: | :---: |
| 75' TURN LANE WITH 150' TAPER ${ }^{2}$ | 1 | EA | \$100,000 | \$100,000 |
| UTILITY RELOCATION ${ }^{3}$ | 0 | EA | \$75,000 | \$0 |
| STORMWATER AND TREATMENT ${ }^{4}$ | 1 | LS | \$75,000 | \$75,000 |
| WORK ZONE TRAFFIC CONTROL | 1 | LS | \$50,000 | \$50,000 |
|  | ESTIMATED CONSTRUCTION COST (CONCEPTUAL) |  |  | \$225,000 |
| CONTIGENCY (20\%) | 1 | LS | \$45,000 | \$45,000 |
| DESIGN AND INSPECTION (25\%) | 1 | LS | \$56,250 | \$60,000 |
|  |  |  | FINAL TOTAL | \$330,000 |

${ }^{2}$ INCLUDES TYPICAL COST FOR PAVEMENT, CURB, EARTHWORK, DRAINAGE, LANDSCAPING, ETC., FOR A 75 ' TURN LANE WITH 150 ' TAPER.
${ }^{3}$ electric and gas relocations are assumed no cost for municipal projects. water and sewer relocations are not present
${ }^{4}$ IMPACTS OVER 5,000 SF WITHIN DEP WATERSHEDS REQUIRE POST STORMWATER TREATMENT. $\$ 75,000$ ALLOWANCE FOR EXTRA ROW OR WORK REQUIRED.

INTERSECTION REALIGNMENT

| DESCRIPTION | TOTAL QUANTITY | UNIT | UNIT PRICE | TOTAL COST |
| :---: | :---: | :---: | :---: | :---: |
| THREE-WAY INTERSECTION ${ }^{5}$ | 1 | EA | \$350,000 | \$350,000 |
| 75' TURN LANE WITH 150' TAPER ${ }^{6}$ | 1 | EA | \$100,000 | \$100,000 |
| ADDITONAL EARTHWORK (ABOVE AND BEYOND TYPICAL) | 5,000 | CY | \$20 | \$100,000 |
| UTILITY RELOCATION ${ }^{7}$ | 0 | EA | \$75,000 | \$0 |
| WAR MEMORIAL RELOCATION | 1 | LS | \$20,000 | \$20,000 |
| STORMWATER AND TREATMENT ${ }^{8}$ | 1 | LS | \$150,000 | \$150,000 |
| WORK ZONE TRAFFIC CONTROL | 1 | LS | \$150,000 | \$150,000 |
|  | ESTIMATED CONSTRUCTION COST (CONCEPTUAL) |  |  | \$870,000 |
| RIGHT OF WAY (RESIDENTIAL) | 0.087 | ACRE | \$65,000 | \$6,000 |
| RIGHT OF WAY (COMMERCIAL) | 0.021 | ACRE | \$340,000 | \$8,000 |
| CONTIGENCY (20\%) | 1 | LS | \$174,000 | \$175,000 |
| DESIGN AND INSPECTION (25\%) | 1 | LS | \$217,500 | \$220,000 |
|  |  |  | FINAL TOTAL | \$1,280,000 |

${ }^{5}$ INCLUDES TYPICAL COST FOR PAVEMENT, CURB, EARTHWORK, DRAINAGE, LANDSCAPING, ETC., FOR A THREE WAY INTERSECTION.
${ }^{6}{ }^{7}$ INCLUDES TYPICAL COST FOR PAVEMENT, CURB, EARTHWORK, DRAINAGE, LANDSCAPING, ETC., FOR A 75 ' TURN LANE WITH 150 ' TAPER.
${ }^{7}$ electric and gas relocations are assumed no cost for municipal projects. water and sewer relocations are not present
${ }^{8}$ IMPACTS OVER 5,000 SF WITHIN DEP WATERSHEDS REQUIRE POST STORMWATER TREATMENT. \$150,000 ALLOWANCE FOR EXTRA ROW OR WORK REQUIRED.

SINGLE LANE ROUNDABOUT (120 FT DIAMETER)

| DESCRIPTION | TOTAL QUANTITY | UNIT | UNIT PRICE | TOTAL COST |
| :---: | :---: | :---: | :---: | :---: |
| SINGLE LANE ROUNDABOUT ${ }^{9}$ | 1 | EA | \$750,000 | \$750,000 |
| ADDITONAL EARTHWORK (ABOVE AND BEYOND TYPICAL) | 10,000 | CY | \$20 | \$200,000 |
| UTILITY RELOCATION ${ }^{10}$ | 0 | EA | \$75,000 | \$0 |
| WAR MEMORIAL RELOCATION | 1 | LS | \$20,000 | \$20,000 |
| STORMWATER AND TREATMENT ${ }^{11}$ | 1 | LS | \$175,000 | \$175,000 |
| WORK ZONE TRAFFIC CONTROL | 1 | LS | \$150,000 | \$150,000 |
|  | ESTIMATED CONSTRUCTION COST (CONCEPTUAL) |  |  | \$1,295,000 |
| RIGHT OF WAY (RESIDENTIAL) | 1 | LS | \$285,000 | \$285,000 |
| RIGHT OF WAY (COMMERCIAL) | 1 | LS | \$380,000 | \$380,000 |
| CONTIGENCY (20\%) | 1 | LS | \$259,000 | \$260,000 |
| DESIGN AND INSPECTION (25\%) | 1 | LS | \$323,750 | \$325,000 |
|  |  |  | FINAL TOTAL | \$2,545,000 |

${ }^{9}$ INCLUDES TYPICAL COST FOR PAVEMENT, CURB, EARTHWORK, DRAINAGE, LANDSCAPING, ETC., FOR A SINGLE LANE ROUNDABOUT.
${ }^{10}$ ELECTRIC AND GAS RELOCATIONS ARE ASSUMED NO COST FOR MUNICIPAL PROJECTS. WATER AND SEWER RELOCATIONS ARE NOT PRESENT•
${ }^{11}$ IMPACTS OVER 5,000 SF WITHIN DEP WATERSHEDS REQUIRE POST STORMWATER TREATMENT. \$175,000 ALLOWANCE FOR EXTRA ROW OR WORK REQUIRED.




## SUMMARY OF INTERSECTION EVALUATION SECOR RD/BRYANT POND RD AND WOOD ST

## Existing Conditions:

This intersection is currently an all-way stop controlled 4-legged intersection, with turn lanes, of approximately 175 feet, on the eastbound, westbound and southbound approaches. Wood Street northbound is posted as 40 mph , but the other 3 approaches; Bryant Pond Rd (eastbound), Secor Rd (westbound) and Wood St (southbound) are all posted as 30 mph .

In reviewing the existing traffic operations, the intersection operated at an overall LOS C with less than 22 seconds per vehicle of delay in both the AM and PM peak hours. No approach operates worse than LOS C in either peak, except for the southbound approach in the PM peak, which operates at LOS D with a 0.83 volume to capacity ratio in the PM peak. Level of services and delays meet acceptable standards. An Intersection Evaluation worksheet, showing geometric details, the existing traffic volumes, and a summary of the capacity analyses is attached.

## Signal Warrant Analysis:

The signal warrant analysis revealed that the Warrant 1 (8-hour criteria) was met for 5 hours of the day, the Warrant 2 (4-hour criteria) was met for 1 hour of the day and the Warrant 3 (peak hour criteria) was not met by any hour of the day. Additionally, fewer than 5 accidents per year occur at this location, so Warrant 7 (Crash Experience) is not satisfied either. As a result, a traffic signal, or similar treatment such as a roundabout is not justified at this time. See attached signal warrant analysis worksheets for more details.

## Accident Analysis:

For the 3-year period studied (2016-2018), 8 accidents were reported at this intersection, the majority of these accidents were rear end and right angle and one resulted in an injury. The calculated accident rate is 0.63 accidents per Million Entering Vehicles (MEV), which is nearly 4 times the statewide average accident rate for similar intersection on State roads. A review of the accident types didn't reveal any particular deficiencies as a cause for the high rate, but the rightangle accidents are of particular concern, as they should not be occurring at an all-way stop intersection unless drivers are disregarding or not seeing the traffic control signs. The accidents types and severity are summarized in the table below, and accident records are attached.

ACCIDENT SUMMARY

| Accident Type | Number of Occurrences | Accident Severity | Number of Occurrences |
| :--- | :---: | :--- | :---: |
| Right Angle | 3 | Fatality | 0 |
| Rear End | 3 | Personal Injury | 1 |
| Backing | 1 | Property Damage Only | 5 |
| Unknown | 1 | Non-Reportable | 2 |
|  | 8 |  | 8 |
|  |  |  |  |

## Field Condition and Right of Way Review:

Sight distances are more than adequate and there are no horizontal or vertical curvature issues near the intersection. There is ample right-of-way to fit a single lane roundabout at this location, though a roundabout would require the relocation of some overhead utilities and poles. It was noticed in the field that a speed limit ends sign for the 40 mph posted speed limit northbound has been placed approximately 300 foot before the intersection, which can confuse drivers; ending the speed limit would indicate to drivers that they could go up to 55 mph , even though all approaches are signed 30 mph at the intersection. Regardless of what improvements are made, that sign should be removed and a 30 mph sign substituted in it's place, or at a bare minimum, remove the sign and replace it with nothing. Either would be better than the sign currently in place.

## Design Alternative Consideration:

Capacity is currently not an issue and level of service is well within an acceptable range, yet the presence of several right-angle accidents is a safety concern. Both a traffic signal and roundabout were analyzed for comparative purposes at this location and it was found that the signal would yield an overall LOS B in the morning and LOS A in the evening, while the Roundabout would yield an overall LOS A for all hours of the day. With that said, it should be noted that a traffic signal would increase some of the queue lengths and would not reduce the chance of right-angle accidents. In fact, it could increase the severity of such accidents, as vehicles won't all be required to stop, which would raise vehicle speeds going through the intersection. As such, a traffic signal is not a good option for this location. A roundabout, on the other hand, would reduce the chance of rear end accidents, reducing queues and the amount of time a queue is present, and it would eliminate all right-angle accidents. Given the accident types present at this location, a roundabout should result in a safer condition. See Figure 11 for a roundabout concept sketch for this location.

## Conceptual Cost Estimate:

Based on our past experience with similar projects, knowledge of construction pricing in this region of New York State and our understanding of the issues, it is estimated that a traffic signal would cost approximately $\$ 250,000$ and a roundabout would cost approximately $\$ 1,670,000$. These costs include construction of all improvements, wetland mitigation, and costs for design and inspection. A breakdown of the big picture cost items is attached.

## Summary \& Conclusion:

The existing intersection appears to operate acceptably with level of service, delays and capacity all within acceptable levels. Traffic volumes are not overly high and the existing traffic control is appropriate for the volumes present. However, there is some concern that too many right-angle accidents may be occurring at this location. A traffic signal would not correct the right-angle accident issue, but a roundabout would. Since the traffic is not high enough to warrant a traffic signal, or roundabout, and the number of accidents occurring isn't high enough to trigger the satisfaction of the crash history signal warrant, it is recommended that no change in traffic control is made at this time, unless the County wishes to eliminate right angle accidents at this location. If so, a roundabout would be the best improvement to achieve that goal. In any case, the "End 40 mph Speed Zone" sign on the northbound approach should be removed or replaced with a 30 mph sign.



Secor Rd \& Wood St

## Mahopac NY

Wednesday, September 11, 2019

|  |  |  | Southbound Wood St |  |  |  |  | Westbound Secor Rd |  |  |  |  | Northbound Wood St |  |  |  |  | Eastbound yant Pond |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | U Turns | Left Turns | Straight | Right |  | U Turns | Left Turns | Straight | Right |  | U Turns | Left Turns | Straight | Right |  | U Turns | Left Turns | Straight | Right | Peds/ |  |
| 12:00 AM | 0 | 0 | Through 0 | Turns 0 | Bicycles 0 | 0 | 0 | Through 0 | Turns 0 | Bicycles 0 | 0 | 0 | Through 0 | Turns 0 | Bicycles 0 | 0 | 0 | Through 0 | Turns 0 | Bicycles 0 | 0 |
| 12:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:00 AM | 0 | 1 | 1 | 46 | 0 | 0 | 2 | 124 | 4 | 0 | 0 | 4 | 1 | 4 | 0 | 0 | 6 | 55 | 2 | 0 | 250 |
| 7:15 AM | 0 | 2 | 1 | 46 | 0 | 0 | 5 | 109 | 1 | 0 | 0 | 8 | 0 | 5 | 0 | 0 | 7 | 65 | 11 | 0 | 260 |
| 7:30 AM | 0 | 3 | 2 | 32 | 1 | 0 | 6 | 99 | 1 | 0 | 0 | 8 | 0 | 3 | 0 | 0 | 7 | 68 | 7 | 0 | 236 |
| 7:45 AM | 0 | 1 | 3 | 36 | 0 | 0 | 4 | 85 | 1 | 0 | 0 | 5 | 1 | 5 | 0 | 0 | 3 | 79 | 10 | 0 | 233 |
| Hourly Total | 0 | 7 | 7 | 160 | 1 | 0 | 17 | 417 | 7 | 0 | 0 | 25 | 2 | 17 | 0 | 0 | 23 | 267 | 30 | 0 | 979 |

Secor Rd \& Wood St
Mahopac NY
Wednesday, September 11, 2019

|  |  |  | Southbound Wood St |  |  |  |  | Westbound Secor Rd |  |  |  |  | Northbound Wood St |  |  | Eastbound Bryant Pond Rd |  |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | U Turns | Left Turns | Straight | Right |  | U Turns | Left Turns | Straight |  | Peds/ | U Turns | Left Turns | Straight | Right | Peds/ | U Turns | Left Turns | Straight |  | Peds/ |  |
|  |  |  | Through | Turns | Bicycles |  | Left Turns | Through | Turns | Bicycles |  |  | Through | Turns | Bicycles |  |  | Through | Turns | Bicycles |  |
| 8:00 AM | 0 | 2 | 3 | 32 | 0 | 0 | 5 | 98 | 1 | 0 | 0 | 3 | 1 | 7 | 0 | 0 | 5 | 47 | 7 | 0 | 211 |
| 8:15 AM | 0 | 0 | 1 | 30 | 0 | 0 | 9 | 90 | 0 | 0 | 0 | 5 | 1 | 9 | 0 | 0 | 14 | 52 | 7 | 0 | 218 |
| 8:30 AM | 0 | 3 | 0 | 22 | 0 | 0 | 4 | 59 | 4 | 0 | 0 | 9 | 0 | 6 | 0 | 0 | 11 | 47 | 4 | 0 | 169 |
| 8:45 AM | 0 | 7 | 3 | 28 | 0 | 0 | 4 | 65 | 1 | 0 | 0 | 6 | 1 | 6 | 0 | 0 | 10 | 48 | 6 | 0 | 185 |
| Hourly Total | 0 | 12 | 7 | 112 | 0 | 0 | 22 | 312 | 6 | 0 | 0 | 23 | 3 | 28 | 0 | 0 | 40 | 194 | 24 | 0 | 783 |
| 9:00 AM | 0 | 5 | 2 | 29 | 0 | 0 | 4 | 62 | 1 | 0 | 0 | 6 | 4 | 8 | 0 | 0 | 8 | 35 | 1 | 0 | 165 |
| 9:15 AM | 0 | 3 | 1 | 21 | 0 | 0 | 6 | 57 | 1 | 0 | 0 | 4 | 1 | 5 | 0 | 0 | 13 | 47 | 5 | 0 | 164 |
| 9:30 AM | 0 | 1 | 3 | 13 | 0 | 0 | 9 | 60 | 4 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 8 | 34 | 5 | 0 | 143 |
| 9:45 AM | 0 | 3 | 0 | 11 | 0 | 1 | 9 | 52 | 1 | 0 | 0 | 5 | 0 | 5 | 0 | 0 | 9 | 27 | 3 | 0 | 126 |
| Hourly Total | 0 | 12 | 6 | 74 | 0 | 1 | 28 | 231 | 7 | 0 | 0 | 21 | 5 | 18 | 0 | 0 | 38 | 143 | 14 | 0 | 598 |
| 10:00 AM | 0 | 3 | 2 | 11 | 0 | 0 | 5 | 34 | 3 | 0 | 0 |  | 0 | 2 | 0 | 0 | 9 | 33 | 6 | 0 | 114 |
| 10:15 AM | 0 | 4 | 0 | 10 | 0 | 0 | 3 | 50 | 2 | 0 | 0 | 8 | 0 | 6 | 0 | 0 | 9 | 44 | 5 | 0 | 141 |
| 10:30 AM | 0 | 4 | 1 | 7 | 0 | 0 | 5 | 30 | 3 | 0 | 0 | 8 | 1 | 4 | 0 | 0 | 3 | 36 | 1 | 0 | 103 |
| 10:45 AM | 0 | 2 | 2 | 8 | 0 | 0 | 6 | 48 | 4 | 0 | 0 | 6 | 2 | 9 | 0 | 0 | 14 | 28 | 3 | 0 | 132 |
| Hourly Total | 0 | 13 | 5 | 36 | 0 | 0 | 19 | 162 | 12 | 0 | 0 | 28 | 3 | 21 | 0 | 0 | 35 | 141 | 15 | 0 | 490 |
| 11:00 AM | 0 | 7 | 1 | 11 | 0 | 0 | 9 | 41 | 1 | 0 | 0 | 4 | 2 | 8 | 0 | 0 | 4 | 43 | 1 | 0 | 132 |
| 11:15 AM | 0 | 2 | 1 | 18 | 0 | 0 | 4 | 42 | 1 | 0 | 0 | 2 | 3 | 7 | 0 | 0 | 8 | 48 | 9 | 0 | 145 |
| 11:30 AM | 0 | 0 | 1 | 8 | 0 | 0 | 1 | 32 | 1 | 0 | 0 | 1 | 3 | 4 | 0 | 0 | 8 | 34 | 8 | 0 | 101 |
| 11:45 AM | 0 | 1 | 3 | 12 | 0 | 0 | 5 | 42 | 3 | 0 | 0 | 3 | 2 | 8 | 0 | 0 | 7 | 40 | 6 | 0 | 132 |
| Hourly Total | 0 | 10 | 6 | 49 | 0 | 0 | 19 | 157 | 6 | 0 | 0 | 10 | 10 | 27 | 0 | 0 | 27 | 165 | 24 | 0 | 510 |
| 12:00 PM | 0 | 1 | 2 | 16 | 0 | 0 | 2 | 44 | 0 | 0 | 0 | 3 | 2 | 5 | 0 | 0 | 6 | 43 | 1 | 0 | 125 |
| 12:15 PM | 0 | 1 | 2 | 12 | 0 | 0 | 3 | 47 | 4 | 0 | 0 | 7 | 0 | 4 | 1 | 1 | 10 | 40 | 2 | 0 | 133 |
| 12:30 PM | 0 | 0 | 1 | 9 | 0 | 0 | 9 | 36 | 3 | 0 | 0 | 6 | 4 | 7 | 0 | 0 | 9 | 30 | 1 | 0 | 115 |
| 12:45 PM | 0 | 1 | 3 | 6 | 0 | 0 | 11 | 51 | 2 | 0 | 0 | 4 | 0 | 7 | 0 | 0 | 11 | 42 | 3 | 0 | 141 |
| Hourly Total | 0 | 3 | 8 | 43 | 0 | 0 | 25 | 178 | 9 | 0 | 0 | 20 | 6 | 23 | 1 | 1 | 36 | 155 | 7 | 0 | 514 |
| 1:00 PM | 0 | 0 | 3 | 10 | 0 | 0 | 5 | 39 | 2 | 1 | 0 | 3 | 2 | 1 | 2 | 2 | 15 | 40 | 6 | 0 | 128 |
| 1:15 PM | 0 | 2 | 2 | 6 | 0 | 0 | 6 | 38 | 1 | 0 | 0 | 9 | 1 | 7 | 0 | 0 | 11 | 44 | 10 | 0 | 137 |
| 1:30 PM | 0 | 1 | 1 | 13 | 0 | 0 | 4 | 38 | 4 | 0 | 0 | 7 | 2 | 8 | 0 | 0 | 8 | 35 | 3 | 0 | 124 |
| 1:45 PM | 0 | 3 | 4 | 9 | 0 | 0 | 4 | 55 | 2 | 0 | 0 | 4 | 3 | 2 | 0 | 0 | 3 | 32 | 3 | 0 | 124 |
| Hourly Total | 0 | 6 | 10 | 38 | 0 | 0 | 19 | 170 | 9 | 1 | 0 | 23 | 8 | 18 | 2 | 2 | 37 | 151 | 22 | 0 | 513 |
| 2:00 PM | 0 | 5 | 2 | 10 | 0 | 0 | 3 | 58 | 3 | 0 | 0 | 8 | 0 | 4 | 0 | 0 | 11 | 46 | 7 | 0 | 157 |
| 2:15 PM | 0 | 1 | 2 | 8 | 2 | 0 | 8 | 49 | 4 | 0 | 0 | 6 | 3 | 13 | 0 | 0 | 10 | 49 | 4 | 0 | 157 |
| 2:30 PM | 0 | 3 | 5 | 14 | 0 | 0 | 2 | 47 | 6 | 0 | 0 | 6 | 5 | 3 | 0 | 0 | 20 | 55 | 7 | 0 | 173 |
| 2:45 PM | 0 | 2 | 3 | 6 | 0 | 0 | 5 | 60 | 7 | 0 | 0 | 8 | 3 | 7 | 0 | 0 | 20 | 66 | 5 | 0 | 192 |
| Hourly Total | 0 | 11 | 12 | 38 | 2 | 0 | 18 | 214 | 20 | 0 | 0 | 28 | 11 | 27 | 0 | 0 | 61 | 216 | 23 | 0 | 679 |
| 3:00 PM | 0 | 1 | 1 | 11 | 0 | 0 | 9 | 71 | 2 | 0 | 0 | 4 | 5 | 13 | 0 | 0 | 18 | 77 | 6 | 0 | 218 |
| 3:15 PM | 0 | 3 | 3 | 22 | 0 | 0 | 3 | 52 | 7 | 0 | 0 | 7 | 2 | 7 | 0 | 0 | 29 | 71 | 6 | 0 | 212 |
| 3:30 PM | 0 | 1 | 1 | 13 | 0 | 0 | 4 | 80 | 2 | 0 | 0 | 11 | 4 | 6 | 0 | 0 | 24 | 81 | 10 | 0 | 237 |
| 3:45 PM | 0 | 2 | 1 | 19 | 0 | 0 | 9 | 62 | 4 | 0 | 0 | 9 | 6 | 11 | 0 | 0 | 28 | 79 | 8 | 0 | 238 |
| Hourly Total | 0 | 7 | 6 | 65 | 0 | 0 | 25 | 265 | 15 | 0 | 0 | 31 | 17 | 37 | 0 | 0 | 99 | 308 | 30 | 0 | 905 |

Secor Rd \& Wood St
Mahopac NY
Wednesday, September 11, 2019

|  |  |  | Southbound Wood St |  |  |  |  | Westbound Secor Rd |  |  |  | 11, 2019 | Northbound Wood St |  |  |  |  | Eastbound yant Pond |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | U Turns | Left Turns | Straight |  |  | U Turns | Left Turns | Straight |  |  | U Turns | Left Turns | Straight |  |  | U Turns | Left Turns | Straight |  |  |  |
|  |  | Lefturns | Through | Turns | Bicycles |  |  | Through | Turns | Bicycles |  |  | Through | Turns | Bicycles |  |  | Through | Turns | Bicycles |  |
| 4:00 PM 4:15 PM | 0 | 1 | 1 | 13 | 0 | 0 | 11 6 | 55 81 | 3 | 0 | 0 | 9 13 | 6 | 9 | 4 0 | 0 | 37 34 | 88 | 6 | 0 | 239 |
| 4:30 PM | 0 | 3 2 | 2 | 20 17 | 0 | 0 | 6 7 | 81 59 | 2 2 | 0 | 0 | 13 12 | 2 | 8 | 0 | 0 | 34 31 | 88 101 | 5 9 | 0 | 264 252 |
| 4:45 PM | 0 | 0 | 3 | 12 | 0 | 0 | 10 | 67 | 6 | 0 | 0 | 12 | 3 | 10 | 0 | 0 | 31 | 98 | 8 | 1 | 260 |
| Hourly Total | 0 | 6 | 10 | 62 | 0 | 0 | 34 | 262 | 13 | 0 | 0 | 46 | 15 | 31 | 4 | 0 | 133 | 375 | 28 | 1 | 1015 |
| 5:00 PM | 0 | 3 | 3 | 8 | 0 | 0 | 9 | 75 | 3 | 0 | 0 | 4 | 4 | 5 | 0 | 0 | 31 | 95 | 14 | 0 | 254 |
| 5:15 PM | 0 | 7 | 1 | 17 | 0 | 0 | 11 | 85 | 3 | 0 | 0 | 14 | 6 | 15 | 0 | 0 | 32 | 106 | 10 | 1 | 307 |
| 5:30 PM | 0 | 4 | 0 | 14 | 0 | 0 | 4 | 78 | 3 | 1 | 0 | 12 | 4 | 14 | 0 | 0 | 37 | 96 | 11 | 0 | 277 |
| 5:45 PM | 0 | 5 | 2 | 16 | 0 | 0 | 10 | 67 | 2 | 0 | 0 | 11 | 2 | 8 | 0 | 0 | 28 | 75 | 8 | 0 | 234 |
| Hourly Total | 0 | 19 | 6 | 55 | 0 | 0 | 34 | 305 | 11 | 1 | 0 | 41 | 16 | 42 | 0 | 0 | 128 | 372 | 43 | 1 | 1072 |
| 6:00 PM | 0 | 3 | 0 | 15 | 0 | 0 | 8 | 70 | 1 | 0 | 0 | 26 | 4 | 7 | 0 | 0 | 23 | 98 | 15 | 0 | 270 |
| 6:15 PM | 0 | 3 | 1 | 16 | 0 | 0 | 6 | 61 | 7 | 0 | 0 | 5 | 3 | 6 | 0 | 0 | 22 | 83 | 8 | 0 | 221 |
| 6:30 PM | 0 | 4 | 4 | 10 | 2 | 0 | 8 | 39 | 7 | 0 | 0 | 9 | 6 | 12 | 0 | 0 | 42 | 110 | 9 | 0 | 260 |
| 6:45 PM | 0 | 2 | 1 | 13 | 0 | 0 | 11 | 49 | 8 | 0 | 0 | 8 | 2 | 10 | 0 | 0 | 29 | 97 | 13 | 0 | 243 |
| Hourly Total | 0 | 12 | 6 | 54 | 2 | 0 | 33 | 219 | 23 | 0 | 0 | 48 | 15 | 35 | 0 | 0 | 116 | 388 | 45 | 0 | 994 |
| 7:00 PM | 0 | 1 | 3 | 9 | 0 | 0 | 13 | 49 | 6 | 0 | 0 | 8 | 4 | 5 | 0 | 0 | 26 | 84 | 9 | 0 | 217 |
| 7:15 PM | 0 | 2 | 1 | 4 | 0 | 0 | 9 | 46 | 3 | 0 | 0 | 6 | 1 | 8 | 1 | 0 | 17 | 60 | 4 | 0 | 161 |
| 7:30 PM | 0 | 5 | 1 | 6 | 0 | 0 | 6 | 39 | 2 | 0 | 0 | 4 | 1 | 2 | 1 | 0 | 19 | 63 | 6 | 0 | 154 |
| 7:45 PM | 0 | 2 | 1 | 6 | 0 | 0 | 6 | 27 | 3 | 0 | 0 | 2 | 3 | 2 | 0 | 0 | 20 | 65 | 6 | 0 | 143 |
| Hourly Total | 0 | 10 | 6 | 25 | 0 | 0 | 34 | 161 | 14 | 0 | 0 | 20 | 9 | 17 | 2 | 0 | 82 | 272 | 25 | 0 | 675 |
| 8:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Hourly Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| daily total | 0 | 128 | 95 | 811 | 5 | 1 | 327 | 3053 | 152 | 2 | 0 | 364 | 120 | 341 | 9 | 3 | 855 | 3147 | 330 | 2 | 9727 |
| Cars | 0 | 123 | 88 | 803 | 2 | 1 | 310 | 2981 | 144 | 0 | 0 | 356 | 119 | 322 | 9 | 3 | 846 | 3066 | 320 | 0 | 9482 |
| Heavy Vehicles | 0 | 5 | 7 | 8 | 3 | 0 | 17 | 72 | 8 | 2 | 0 | 8 | 1 | 19 | 0 | 0 | 9 | 81 | 10 | 2 | 245 |
| Heavy Vehicle \% | 0.00\% | 3.91\% | 7.37\% | 0.99\% | 60.00\% | 0.00\% | 5.20\% | 2.36\% | 5.26\% | 100.00\% | 0.00\% | 2.20\% | 0.83\% | 5.57\% | 0.00\% | 0.00\% | 1.05\% | 2.57\% | 3.03\% | 100.00\% | 2.52\% |

Secor Rd \& Wood St
Mahopac NY
Wednesday, September 11, 2019


| Vehicles Entering 1034 |  |  | Vehicles ExitingIntersection 1127 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Suthbound |  |  |  |  |  |
| Cars | 803 | 88 | 123 | 0 | 2 |
| Heavy | 8 | 7 | 5 | 0 | 3 |
| Total | 811 | 95 | 128 | 0 | 5 |



| Cars | Heavy | Total |  | VehiclesEnteringIntersection3533 | Total Vehicles on Leg 7150 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 144 | 8 | 152 |  |  |  |
| 2981 | 72 | 3053 |  |  |  |
| 310 | 17 | 327 |  |  |  |
| 1 | 0 | 1 |  | $\begin{array}{\|c\|} \text { Exiting } \\ \text { Intersection } \end{array}$ |  |
| 0 | 2 | 2 |  | 3617 |  |



TRAFFIC SIGNAL WARRANT SUMMARY

| Project: <br> Location: | Putnam County Roundabout Evaluation | Condition: |  | 2019 Existing Condition |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Location: | Secor Rd \& Wood St |  |  | Date: September | , 2019 |
| Major Street: | Secor Rd | Lanes: | 1 | Critical Approach Speed: | 40 mph |
| Minor Street: | Wood St | Lanes: | 1 |  |  |

## Volume Level Criteria

1. Is the critical speed of major street traffic greater than 40 mph ?
2. Is the intersection in a built-up area of an isolated community with population less than 10,000 ?

|  | No |
| :---: | :---: |
|  | No |
| Criteria used: | 100\% |

## WARRANT 1 - EIGHT HOUR VEHICULAR VOLUME

Warrant 1 Satisfied: $\qquad$ NO
Warrant 1 is satisfied if EITHER Condition A OR Condition B is $100 \%$ satisfied.
Warrant 1 is also satisfied if BOTH Condition A AND Condition B are satisfied to the $80 \%$ volume level.

|  |  |  | Condition 1A - Minimum Vehicular Volume <br> ( X indicates that criteria is met for specified condition) |  |  |  | Condition 1B - Interuption of Continuous Traffic ( X indicates that criteria is met for specified condition) |  |  |  | Total Satisfied Hours (8 required) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1 | 5 | 2 |  |  |  |  |
| Minimum Volume Criteria: |  |  |  |  |  |  | 500 | 150 | 400 | 120 | 750 | 75 | 600 | 60 | Condition | Condition | 80\% for |
| $\begin{aligned} & \hline \text { Start } \\ & \text { Time } \end{aligned}$ | Major St. <br> Volume ${ }^{1}$ | Minor St. Volume ${ }^{2}$ | $\begin{gathered} \hline \text { Major St. } \\ 100 \% \end{gathered}$ | Minor St. 100\% | $\begin{gathered} \text { Major St. } \\ 80 \% \end{gathered}$ | Minor St. 80\% | $\begin{gathered} \text { Major St. } \\ \text { 100\%\% } \end{gathered}$ | $\begin{gathered} \hline \text { Minor St. } \\ 100 \% \end{gathered}$ | $\begin{gathered} \hline \text { Major St. } \\ 80 \% \end{gathered}$ | $\begin{gathered} \text { Minor St. } \\ 80 \% \end{gathered}$ | 1A <br> Satisfied | 1B <br> Satisfied | Both Satisfied |
| 12:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 1:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 2:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 3:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 4:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 5:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 6:00 AM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 7:00 AM | 799 | 183 | X | X | X | X | X | X | X | X | 1 | 1 | 1 |
| 8:00 AM | 628 | 138 | X | - | X | X | - | X | X | X | - | - | 1 |
| 9:00 AM | 485 | 97 | - | - | X | - | - | X | - | X | - | - | - |
| 10:00 AM | 403 | 57 | - | - | X | - | - | - | - | - | - | - | - |
| 11:00 AM | 418 | 68 | - | - | X | - | - | - | - | X | - | - | - |
| 12:00 PM | 432 | 57 | - | - | X | - | - | - | - | - | - | - | - |
| 1:00 PM | 431 | 57 | - | - | X | - | - | - | - | - | - | - | - |
| 2:00 PM | 580 | 69 | X | - | X | - | - | - | - | X | - | - | - |
| 3:00 PM | 779 | 89 | X | - | X | - | X | X | X | X | - | 1 | - |
| 4:00 PM | 887 | 97 | X | - | X | - | X | X | X | X | - | 1 | - |
| 5:00 PM | 938 | 104 | X | - | X | - | X | X | X | X | - | 1 | - |
| 6:00 PM | 865 | 103 | X | - | X | - | X | X | X | X | - | 1 | - |
| 7:00 PM | 617 | 48 | X | - | X | - | - | - | X | - | - | - | - |
| 8:00 PM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 9:00 PM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 10:00 PM |  |  | - | - | - | - | - | - | - | - | - | - | - |
| 11:00 PM |  |  | - | - | - | - | - | - | - | - | - | - | - |

${ }^{1}$ Major Street Volume is the total combined volume of both mainline approaches.
${ }^{2}$ Minor Street volumes is the highest single side street approach volume.

## Note: Right turn traffic was removed from side street volume and only one of the two available lanes was considered in the Warrant analysis.

WARRANT 2 - FOUR HOUR VEHICULAR VOLUME
Warrant is satisfied if four (4) or more hours satisfy the volume requirements depicted on the four hour warranting graph (see page 2).

| Warrant 2 Satisfied: | NO |
| ---: | ---: |
| No. of Points Above Criteria Curve: | 1 | 1

Warrant is satisfied if any hour satisfy the volume requirements depicted on the peak hour warranting graph (see page 3), and ALL three of the following requirement are met.
$\qquad$
Warrant 3 Satisfied: NO No. of Points Above Criteria Curve: $\qquad$ 0

1. Total stopped time delay on Minor Street equals or exceeds 4 VHD (single lane) or 5 VHD (two lanes):
2. Volume on Minor Street equals or exceeds 100 vehicles (single lane) or 150 vehicles (two lanes):
3. Total intersection volume serviced during the hour equals or exceeds 650 veh. (3-leg) or 800 veh. (4-leg or more):
$\qquad$ VHD Max. $\qquad$

Figure 4C-1. Warrant 2, Four-Hour Vehicular Volume


Note: Points on graph represent hourly volumes. Points above the respective curve satisfy warrant, points below do not satisfy warrant.

Figure 4C-3. Warrant 3, Peak Hour


Note: Points on graph represent hourly volumes. Points above the
respective curve satisfy warrant, points below do not satisfy warrant.

## Accident Location Information System(ALIS)

## Accident Verbal Description

16408_VDR
Date in this report covers the period - 2/29/2016-2/28/2019

## Complete Accident data from NYSDMV is only available thru 2/28/2019 12:00:00 AM

County: Putnam Muni: Putnam Valley(T) Ref. Marker: Street: BRYANT POND RD
AT INTERSECTION WITH WOOD ST
Tue 01:40 AM Persons Killed: 0
Persons Injured: 0
Extent of Injuries:
Police Agency: PUTNAM CO SHERIFF DEPT
Case: 2016-36208155
$\begin{array}{lll}\text { Accident Class: NON-REPORTABLE } & \text { Police Agency: PUTNAM CO SHERIFF DEPT } \\ \text { Type Of Accident: COLLISION WITH MOTOR VEHICLE } & & \text { Traffic Control: STOP SIGN }\end{array}$
Manner of Collision: REAR END
Road Char.: STRAIGHT AND LEVEL
Road Surface Condition: WET
Loc. of Ped/Bicycle: NOT APPLICABLE
Light Condition: DARK-ROADUNLIGHTED

CAR/VAN/PICKUP
Registered Weight:
Num of Occupants: 4
Direction of Travel: EAST
Driver's Age: 18
Action of Ped/Bicycle: NOT APPLICABLE
Veh :1

Public Property Damage: OTHER
Pre-Accd Action: SLOWED OR STOPPING
Apparent Factors: FOLLOWING TOO CLOSELY, PAVEMENT SLIPPERY

CAR/VAN/PICKUP
Registered Weight:
Driver's Age: 21
Direction of Travel: EAST
Public Property Damage: OTHER
Sex: M Citation Issued: N
School Bus Involved: OTHER

Pre-Accd Action: SLOWED OR STOPPING
Apparent Factors: NOT APPLICABLE, NOT APPLICABLE
County: Putnam Muni: Putnam Valley(T) Ref. Marker: Street: SECOR RD
AT INTERSECTION WITH WOOD ST
Sat 11:19 AM Persons Killed: 0
Persons Injured: 0
Extent of Injuries:
State of Registration: NY
Sex: M Citation Issued: N
School Bus Involved: OTHER

Accident Class: PROPERTY DAMAGE
Police Agency: PUTNAM CO SHERIFF DEPT

## Case: 2016-36271026

Type Of Accident: COLLISION WITH MOTOR VEHICLE
Manner of Collision: UNKNOWN
Road Surface Condition: DRY
Road Char.: STRAIGHT AND LEVEL

Loc. of Ped/Bicycle: NOT APPLICABLE
Action of Ped/Bicycle: NOT APPLICABL
OTHER Registered Weight:
Num of Occupants: 0 Driver's Age: Sex:

Direction of Travel: UNKNOWN Public Property Damage: OTHER
Citation Issued:
School Bus Involved: OTHER
Pre-Accd Action: UNKNOWN
Apparent Factors: UNKNOWN, BACKING UNSAFELY

State of Registration: NY Sex: Citation Issued: School Bus Involved: OTHER

Driver's Age:
Public Property Damage: OTHER
Pre-Accd Action: PARKED
Apparent Factors: NOT APPLICABLE, NOTAPPLICABLE



Pre-Accd Action: GOING STRAIGHT AHEAD
Apparent Factors: NOT APPLICABLE, NOT APPLICABLE
County: Putnam Muni: Putnam Valley(T) Ref. Marker: Street: BRYANT POND RD


Pre-Accd Action: GOING STRAIGHT AHEAD
Apparent Factors: NOT APPLICABLE, TRAFFIC CONTROL DEVICES DISREGARDED
County: Putnam Muni: Kent(T) Ref. Marker: Street: HILL AND DALE RD


CAR/VAN/PICKUP
Num of Occupants: 1
Direction of Travel: SOUTH
Pre-Accd Action: GOING STRAIGHT AHEAD
Apparent Factors: DRIVER INATTENTION, NOT APPLICABLE

Driver's Age: 40
Public Property Damage: OTHER

State of Registration: NY
Citation Issued: N
School Bus Involved: OTHER
Public Property Damage: OTHER

Num of Occupants: 3
Direction of Travel: SOUTH
Pre-Accd Action: STOPPED IN TRAFFIC
Apparent Factors: NOT APPLICABLE, NOTAPPLICABLE

| Intersection |  |
| :--- | ---: | :--- |
| Intersection Delay, s/veh | 18.7 |
| Intersection LOS | C |


| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{*}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |  | \& |  |  | $\uparrow$ | 「 |
| Traffic Vol, veh/h | 24 | 280 | 32 | 18 | 438 | 7 | 26 | 2 | 18 | 7 | 7 | 168 |
| Future Vol, veh/h | 24 | 280 | 32 | 18 | 438 | 7 | 26 | 2 | 18 | 7 | 7 | 168 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles, \% | 1 | 1 | 1 | 12 | 2 | 15 | 1 | 1 | 12 | 1 | 14 | 1 |
| Mvmt Flow | 26 | 298 | 34 | 19 | 466 | 7 | 28 | 2 | 19 | 7 | 7 | 179 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| Approach | SE |  |  | NW |  |  | NE |  |  | SW |  |  |
| Opposing Approach | NW |  |  | SE |  |  | SW |  |  | NE |  |  |
| Opposing Lanes | 2 |  |  | 2 |  |  | 2 |  |  | 1 |  |  |
| Conflicting Approach Left | SW |  |  | NE |  |  | SE |  |  | NW |  |  |
| Conflicting Lanes Left | 2 |  |  | 1 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Right | NE |  |  | SW |  |  | NW |  |  | SE |  |  |
| Conflicting Lanes Right | 1 |  |  | 2 |  |  | 2 |  |  | 2 |  |  |
| HCM Control Delay | 15.2 |  |  | 24.6 |  |  | 11.1 |  |  | 12 |  |  |
| HCM LOS | C |  |  | C |  |  | B |  |  | B |  |  |


| Lane | NELn1 | NWLn1 | NWLn2 | SELn1 | SELn2 | SWLn1 | SWLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $57 \%$ | $100 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $50 \%$ | $0 \%$ |
| Vol Thru, \% | $4 \%$ | $0 \%$ | $98 \%$ | $0 \%$ | $90 \%$ | $50 \%$ | $0 \%$ |
| Vol Right, \% | $39 \%$ | $0 \%$ | $2 \%$ | $0 \%$ | $10 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 46 | 18 | 445 | 24 | 312 | 14 | 168 |
| LT Vol | 26 | 18 | 0 | 24 | 0 | 7 | 0 |
| Through Vol | 2 | 0 | 438 | 0 | 280 | 7 | 0 |
| RT Vol | 18 | 0 | 7 | 0 | 32 | 0 | 168 |
| Lane Flow Rate | 49 | 19 | 473 | 26 | 332 | 15 | 179 |
| Geometry Grp | 6 | 7 | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.098 | 0.035 | 0.766 | 0.046 | 0.546 | 0.03 | 0.32 |
| Departure Headway (Hd) | 7.244 | 6.515 | 5.825 | 6.501 | 5.92 | 7.187 | 6.444 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 491 | 549 | 620 | 549 | 607 | 496 | 556 |
| Service Time | 5.339 | 4.264 | 3.574 | 4.256 | 3.675 | 4.955 | 4.212 |
| HCM Lane V/C Ratio | 0.1 | 0.035 | 0.763 | 0.047 | 0.547 | 0.03 | 0.322 |
| HCM Control Delay | 11.1 | 9.5 | 25.2 | 9.6 | 15.6 | 10.2 | 12.2 |
| HCM Lane LOS | B | A | D | A | C | B | B |
| HCM 95th-tile Q | 0.3 | 0.1 | 7 | 0.1 | 3.3 | 0.1 | 1.4 |


|  | $\cdots$ | * | n | $k$ | $\nearrow$ | 4 | $\cdots$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | SEL | SET | NWL | NWT | NET | SWT | SWR |
| Lane Group Flow (vph) | 26 | 332 | 19 | 473 | 49 | 14 | 179 |
| v/c Ratio | 0.06 | 0.34 | 0.04 | 0.50 | 0.09 | 0.03 | 0.27 |
| Control Delay | 7.5 | 8.9 | 7.2 | 11.3 | 9.0 | 11.5 | 4.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 7.5 | 8.9 | 7.2 | 11.3 | 9.0 | 11.5 | 4.1 |
| Queue Length 50th (tt) | 4 | 51 | 3 | 86 | 4 | 2 | 0 |
| Queue Length 95th (ft) | 13 | 95 | 10 | 154 | 25 | 13 | 34 |
| Internal Link Dist (ft) |  | 549 |  | 718 | 564 | 822 |  |
| Turn Bay Length (ft) | 200 |  | 200 |  |  |  | 200 |
| Base Capacity (vph) | 631 | 1442 | 712 | 1391 | 610 | 622 | 736 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.04 | 0.23 | 0.03 | 0.34 | 0.08 | 0.02 | 0.24 |

[^1]| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\hat{\beta}$ |  | \% | F |  |  | ¢ |  |  | $\uparrow$ | 「 |
| Traffic Volume (veh/h) | 24 | 280 | 32 | 18 | 438 | 7 | 26 | 2 | 18 | 7 | 7 | 168 |
| Future Volume (veh/h) | 24 | 280 | 32 | 18 | 438 | 7 | 26 | 2 | 18 | 7 | 7 | 168 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 0.98 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1885 | 1885 | 1885 | 1722 | 1870 | 1870 | 1885 | 1885 | 1885 | 1693 | 1693 | 1885 |
| Adj Flow Rate, veh/h | 26 | 298 | 34 | 19 | 466 | 7 | 28 | 2 | 19 | 7 | 7 | 179 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh, \% | 1 | 1 | 1 | 12 | 2 | 2 | 1 | 1 | 1 | 14 | 14 | 1 |
| Cap, veh/h | 324 | 595 | 68 | 405 | 658 | 10 | 409 | 62 | 202 | 375 | 320 | 594 |
| Arrive On Green | 0.36 | 0.36 | 0.36 | 0.36 | 0.36 | 0.36 | 0.37 | 0.37 | 0.37 | 0.37 | 0.37 | 0.37 |
| Sat Flow, veh/h | 928 | 1661 | 190 | 965 | 1837 | 28 | 690 | 167 | 543 | 618 | 862 | 1598 |
| Grp Volume(v), veh/h | 26 | 0 | 332 | 19 | 0 | 473 | 49 | 0 | 0 | 14 | 0 | 179 |
| Grp Sat Flow(s),veh/h/n | 928 | 0 | 1851 | 965 | 0 | 1865 | 1400 | 0 | 0 | 1480 | 0 | 1598 |
| Q Serve(g_s), s | 0.9 | 0.0 | 5.2 | 0.6 | 0.0 | 8.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.9 |
| Cycle Q Clear(g_c), s | 9.0 | 0.0 | 5.2 | 5.8 | 0.0 | 8.1 | 0.7 | 0.0 | 0.0 | 0.2 | 0.0 | 2.9 |
| Prop In Lane | 1.00 |  | 0.10 | 1.00 |  | 0.01 | 0.57 |  | 0.39 | 0.50 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 324 | 0 | 663 | 405 | 0 | 668 | 673 | 0 | 0 | 696 | 0 | 594 |
| V/C Ratio(X) | 0.08 | 0.00 | 0.50 | 0.05 | 0.00 | 0.71 | 0.07 | 0.00 | 0.00 | 0.02 | 0.00 | 0.30 |
| Avail Cap(c_a), veh/h | 820 | 0 | 1651 | 920 | 0 | 1663 | 792 | 0 | 0 | 822 | 0 | 734 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 14.1 | 0.0 | 9.3 | 11.5 | 0.0 | 10.2 | 7.5 | 0.0 | 0.0 | 7.4 | 0.0 | 8.2 |
| Incr Delay (d2), s/veh | 0.1 | 0.0 | 0.6 | 0.0 | 0.0 | 1.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.3 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.2 | 0.0 | 1.6 | 0.1 | 0.0 | 2.6 | 0.2 | 0.0 | 0.0 | 0.1 | 0.0 | 0.8 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay (d),s/veh | 14.2 | 0.0 | 9.9 | 11.6 | 0.0 | 11.6 | 7.6 | 0.0 | 0.0 | 7.4 | 0.0 | 8.5 |
| LnGrp LOS | B | A | A | B | A | B | A | A | A | A | A | A |
| Approach Vol, veh/h |  | 358 |  |  | 492 |  |  | 49 |  |  | 193 |  |
| Approach Delay, s/veh |  | 10.2 |  |  | 11.6 |  |  | 7.6 |  |  | 8.4 |  |
| Approach LOS |  | B |  |  | B |  |  | A |  |  | A |  |


| Timer - Assigned Phs | 2 | 4 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), s | 18.3 | 18.8 | 18.3 | 18.8 |
| Change Period (Y+Rc), s | 5.0 | 5.0 | 5.0 | 5.0 |
| Max Green Setting (Gmax), s | 33.0 | 17.0 | 33.0 | 17.0 |
| Max Q Clear Time (g_c+11), s | 10.1 | 2.7 | 11.0 | 4.9 |
| Green Ext Time (p_c), s | 3.2 | 0.1 | 2.1 | 0.5 |

## Intersection Summary

HCM 6th Ctrl Delay 10.4

HCM 6th LOS

| Intersection |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 6.1 |  |  |  |  |  |  |  |
| Intersection LOS | A |  |  |  |  |  |  |  |
| Approach |  | SE |  | NW |  | NE |  | SW |
| Entry Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Conflicting Circle Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Adj Approach Flow, veh/h |  | 358 |  | 492 |  | 49 |  | 193 |
| Demand Flow Rate, veh/h |  | 361 |  | 504 |  | 51 |  | 196 |
| Vehicles Circulating, veh/h |  | 36 |  | 56 |  | 334 |  | 524 |
| Vehicles Exiting, veh/h |  | 684 |  | 329 |  | 63 |  | 36 |
| Ped Vol Crossing Leg, \#/h |  | 0 |  | 0 |  | 0 |  | 0 |
| Ped Cap Adj |  | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |
| Approach Delay, s/veh |  | 5.1 |  | 6.5 |  | 4.3 |  | 7.2 |
| Approach LOS |  | A |  | A |  | A |  | A |
| Lane | Left |  | Left |  | Left |  | Left |  |
| Designated Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| Assumed Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| RT Channelized |  |  |  |  |  |  |  |  |
| Lane Util | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |  |
| Follow-Up Headway, s | 2.609 |  | 2.609 |  | 2.609 |  | 2.609 |  |
| Critical Headway, s | 4.976 |  | 4.976 |  | 4.976 |  | 4.976 |  |
| Entry Flow, veh/h | 361 |  | 504 |  | 51 |  | 196 |  |
| Cap Entry Lane, veh/h | 1330 |  | 1303 |  | 982 |  | 809 |  |
| Entry HV Adj Factor | 0.992 |  | 0.976 |  | 0.960 |  | 0.985 |  |
| Flow Entry, veh/h | 358 |  | 492 |  | 49 |  | 193 |  |
| Cap Entry, veh/h | 1319 |  | 1271 |  | 943 |  | 796 |  |
| V/C Ratio | 0.271 |  | 0.387 |  | 0.052 |  | 0.242 |  |
| Control Delay, s/veh | 5.1 |  | 6.5 |  | 4.3 |  | 7.2 |  |
| LOS | A |  | A |  | A |  | A |  |
| 95th \%tile Queue, veh | 1 |  | 2 |  | 0 |  | 1 |  |


| Intersection |  |
| :--- | ---: |
| Intersection Delay, s/veh | 21.3 |
| Intersection LOS | C |


| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  | 7 | F |  |  | \$ |  |  | \$ $\uparrow$ | 7 |
| Traffic Vol, veh/h | 138 | 415 | 45 | 36 | 320 | 16 | 44 | 18 | 46 | 15 | 7 | 54 |
| Future Vol, veh/h | 138 | 415 | 45 | 36 | 320 | 16 | 44 | 18 | 46 | 15 | 7 | 54 |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles, \% | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 6 | 2 | 1 | 1 | 1 |
| Mvmt Flow | 155 | 466 | 51 | 40 | 360 | 18 | 49 | 20 | 52 | 17 | 8 | 61 |
| Number of Lanes | 1 | 1 | 0 | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| Approach | SE |  |  | NW |  |  | NE |  |  | SW |  |  |
| Opposing Approach | NW |  |  | SE |  |  | SW |  |  | NE |  |  |
| Opposing Lanes | 2 |  |  | 2 |  |  | 2 |  |  | 1 |  |  |
| Conflicting Approach Left | SW |  |  | NE |  |  | SE |  |  | NW |  |  |
| Conflicting Lanes Left | 2 |  |  | 1 |  |  | 2 |  |  | 2 |  |  |
| Conflicting Approach Right | NE |  |  | SW |  |  | NW |  |  | SE |  |  |
| Conflicting Lanes Right | 1 |  |  | 2 |  |  | 2 |  |  | 2 |  |  |
| HCM Control Delay | 26 |  |  | 18.3 |  |  | 12.6 |  |  | 10.7 |  |  |
| HCM LOS | D |  |  | C |  |  | B |  |  | B |  |  |


| Lane | NELn1 | NWLn1 | NWLn2 | SELn1 | SELn2 | SWLn1 | SWLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol Left, \% | $41 \%$ | $100 \%$ | $0 \%$ | $100 \%$ | $0 \%$ | $68 \%$ | $0 \%$ |
| Vol Thru, $\%$ | $17 \%$ | $0 \%$ | $95 \%$ | $0 \%$ | $90 \%$ | $32 \%$ | $0 \%$ |
| Vol Right, \% | $43 \%$ | $0 \%$ | $5 \%$ | $0 \%$ | $10 \%$ | $0 \%$ | $100 \%$ |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop |
| Traffic Vol by Lane | 108 | 36 | 336 | 138 | 460 | 22 | 54 |
| LT Vol | 44 | 36 | 0 | 138 | 0 | 15 | 0 |
| Through Vol | 18 | 0 | 320 | 0 | 415 | 7 | 0 |
| RT Vol | 46 | 0 | 16 | 0 | 45 | 0 | 54 |
| Lane Flow Rate | 121 | 40 | 378 | 155 | 517 | 25 | 61 |
| Geometry Grp | 6 | 7 | 7 | 7 | 7 | 7 | 7 |
| Degree of Util (X) | 0.243 | 0.075 | 0.641 | 0.273 | 0.828 | 0.054 | 0.115 |
| Departure Headway (Hd) | 7.209 | 6.656 | 6.114 | 6.342 | 5.766 | 7.913 | 6.846 |
| Convergence, Y/N | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Cap | 496 | 536 | 589 | 564 | 625 | 450 | 520 |
| Service Time | 5.287 | 4.419 | 3.877 | 4.096 | 3.52 | 5.701 | 4.632 |
| HCM Lane V/C Ratio | 0.244 | 0.075 | 0.642 | 0.275 | 0.827 | 0.056 | 0.117 |
| HCM Control Delay | 12.6 | 10 | 19.2 | 11.5 | 30.4 | 11.2 | 10.5 |
| HCM Lane LOS | B | A | C | B | D | B | B |
| HCM 95th-tile Q | 0.9 | 0.2 | 4.6 | 1.1 | 8.7 | 0.2 | 0.4 |


|  | $\cdots$ | k | $\cdots$ | $k$ | $\nearrow$ | 4 | * |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | SEL | SET | NWL | NWT | NET | SWT | SWR |
| Lane Group Flow (vph) | 155 | 517 | 40 | 378 | 76 | 25 | 61 |
| v/c Ratio | 0.23 | 0.42 | 0.08 | 0.32 | 0.12 | 0.05 | 0.10 |
| Control Delay | 8.0 | 8.3 | 7.0 | 7.4 | 7.4 | 13.2 | 5.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 8.0 | 8.3 | 7.0 | 7.4 | 7.4 | 13.2 | 5.4 |
| Queue Length 50th (ft) | 24 | 92 | 6 | 62 | 4 | 4 | 0 |
| Queue Length 95th (ft) | 54 | 159 | 17 | 109 | 30 | 20 | 21 |
| Internal Link Dist (ft) |  | 549 |  | 718 | 564 | 822 |  |
| Turn Bay Length (ft) | 200 |  | 200 |  |  |  | 200 |
| Base Capacity (vph) | 794 | 1458 | 618 | 1418 | 718 | 593 | 675 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.20 | 0.35 | 0.06 | 0.27 | 0.11 | 0.04 | 0.09 |

[^2]| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | F |  | \% | F |  |  | $\uparrow$ |  |  | $\uparrow$ | F |
| Traffic Volume (veh/h) | 138 | 415 | 45 | 36 | 320 | 16 | 4 | 18 | 46 | 15 | 7 | 54 |
| Future Volume (veh/h) | 138 | 415 | 45 | 36 | 320 | 16 | 4 | 18 | 46 | 15 | 7 | 54 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.98 | 1.00 |  | 0.98 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1885 | 1885 | 1885 | 1885 | 1885 | 1885 | 1811 | 1811 | 1811 | 1885 | 1885 | 1885 |
| Adj Flow Rate, veh/h | 155 | 466 | 51 | 40 | 360 | 18 | 4 | 20 | 52 | 17 | 8 | 61 |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Percent Heavy Veh, \% | 1 | 1 | 1 | 1 | 1 | 1 | 6 | 6 | 6 | 1 | 1 | 1 |
| Cap, veh/h | 472 | 717 | 79 | 369 | 765 | 38 | 103 | 151 | 342 | 449 | 184 | 494 |
| Arrive On Green | 0.43 | 0.43 | 0.43 | 0.43 | 0.43 | 0.43 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 | 0.32 |
| Sat Flow, veh/h | 1013 | 1670 | 183 | 891 | 1780 | 89 | 22 | 477 | 1081 | 935 | 583 | 1563 |
| Grp Volume(v), veh/h | 155 | 0 | 517 | 40 | 0 | 378 | 76 | 0 | 0 | 25 | 0 | 61 |
| Grp Sat Flow(s),veh/h/n | 1013 | 0 | 1852 | 891 | 0 | 1869 | 1580 | 0 | 0 | 1518 | 0 | 1563 |
| Q Serve(g_s), s | 5.1 | 0.0 | 8.7 | 1.5 | 0.0 | 5.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.1 |
| Cycle Q Clear(g_c), s | 10.8 | 0.0 | 8.7 | 10.2 | 0.0 | 5.7 | 1.4 | 0.0 | 0.0 | 0.4 | 0.0 | 1.1 |
| Prop In Lane | 1.00 |  | 0.10 | 1.00 |  | 0.05 | 0.05 |  | 0.68 | 0.68 |  | 1.00 |
| Lane Grp Cap (c), veh/h | 472 | 0 | 796 | 369 | 0 | 803 | 596 | 0 | 0 | 634 | 0 | 494 |
| V/C Ratio(X) | 0.33 | 0.00 | 0.65 | 0.11 | 0.00 | 0.47 | 0.13 | 0.00 | 0.00 | 0.04 | 0.00 | 0.12 |
| Avail Cap(c_a), veh/h | 885 | 0 | 1553 | 733 | 0 | 1567 | 776 | 0 | 0 | 804 | 0 | 675 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 11.9 | 0.0 | 8.9 | 12.9 | 0.0 | 8.0 | 9.7 | 0.0 | 0.0 | 9.3 | 0.0 | 9.6 |
| Incr Delay (d2), s/veh | 0.4 | 0.0 | 0.9 | 0.1 | 0.0 | 0.4 | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.0 | 0.0 | 2.6 | 0.3 | 0.0 | 1.7 | 0.3 | 0.0 | 0.0 | 0.1 | 0.0 | 0.3 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 12.3 | 0.0 | 9.8 | 13.0 | 0.0 | 8.5 | 9.8 | 0.0 | 0.0 | 9.4 | 0.0 | 9.7 |
| LnGrp LOS | B | A | A | B | A | A | A | A | A | A | A | A |
| Approach Vol, veh/h |  | 672 |  |  | 418 |  |  | 76 |  |  | 86 |  |
| Approach Delay, s/veh |  | 10.4 |  |  | 8.9 |  |  | 9.8 |  |  | 9.6 |  |
| Approach LOS |  | B |  |  | A |  |  | A |  |  | A |  |


| Timer - Assigned Phs | 2 | 4 | 6 | 8 |
| :--- | ---: | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), s | 21.9 | 17.4 | 21.9 | 17.4 |
| Change Period (Y+Rc), s | 5.0 | 5.0 | 5.0 | 5.0 |
| Max Green Setting (Gmax), s | 33.0 | 17.0 | 33.0 | 17.0 |
| Max Q Clear Time (g_c+11), s | 12.2 | 3.4 | 12.8 | 3.1 |
| Green Ext Time (p_c), s | 2.5 | 0.2 | 4.1 | 0.2 |

## Intersection Summary

HCM 6th Ctrl Delay 9.8

HCM 6th LOS

| Intersection |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 7.8 |  |  |  |  |  |  |  |
| Intersection LOS | A |  |  |  |  |  |  |  |
| Approach |  | SE |  | NW |  | NE |  | SW |
| Entry Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Conflicting Circle Lanes |  | 1 |  | 1 |  | 1 |  | 1 |
| Adj Approach Flow, veh/h |  | 672 |  | 418 |  | 121 |  | 86 |
| Demand Flow Rate, veh/h |  | 680 |  | 422 |  | 123 |  | 87 |
| Vehicles Circulating, veh/h |  | 65 |  | 227 |  | 645 |  | 453 |
| Vehicles Exiting, veh/h |  | 475 |  | 541 |  | 100 |  | 196 |
| Ped Vol Crossing Leg, \#/h |  | 0 |  | 0 |  | 0 |  | 0 |
| Ped Cap Adj |  | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |
| Approach Delay, s/veh |  | 8.5 |  | 7.3 |  | 7.1 |  | 5.2 |
| Approach LOS |  | A |  | A |  | A |  | A |
| Lane | Left |  | Left |  | Left |  | Left |  |
| Designated Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| Assumed Moves | LTR |  | LTR |  | LTR |  | LTR |  |
| RT Channelized |  |  |  |  |  |  |  |  |
| Lane Util | 1.000 |  | 1.000 |  | 1.000 |  | 1.000 |  |
| Follow-Up Headway, s | 2.609 |  | 2.609 |  | 2.609 |  | 2.609 |  |
| Critical Headway, s | 4.976 |  | 4.976 |  | 4.976 |  | 4.976 |  |
| Entry Flow, veh/h | 680 |  | 422 |  | 123 |  | 87 |  |
| Cap Entry Lane, veh/h | 1291 |  | 1095 |  | 715 |  | 869 |  |
| Entry HV Adj Factor | 0.989 |  | 0.991 |  | 0.982 |  | 0.988 |  |
| Flow Entry, veh/h | 672 |  | 418 |  | 121 |  | 86 |  |
| Cap Entry, veh/h | 1277 |  | 1085 |  | 702 |  | 859 |  |
| V/C Ratio | 0.527 |  | 0.386 |  | 0.172 |  | 0.100 |  |
| Control Delay, s/veh | 8.5 |  | 7.3 |  | 7.1 |  | 5.2 |  |
| LOS | A |  | A |  | A |  | A |  |
| 95th \%tile Queue, veh | 3 |  | 2 |  | 1 |  | 0 |  |

Engineering and Construction Services

| Client: Putnam County | GPI No. 2019058.00 |
| :---: | :---: |
| Calculated By: D. Creen | Date: 9/29/2019 |
| Checked By: M. Wieszchowski | Date: 9/30/2019 |

## ACTUATED TRAFFIC SIGNAL WITH NO GEOMETRIC IMPROVEMENTS

| DESCRIPTION | TOTAL QUANTITY | UNIT | UNIT PRICE | TOTAL COST |
| :---: | :---: | :---: | :---: | :---: |
| ACTUATED TRAFFIC SIGNAL ${ }^{1}$ | 1 | EA | \$150,000 | \$150,000 |
| WORK ZONE TRAFFIC CONTROL | 1 | LS | \$20,000 | \$20,000 |
|  | ESTIMATED CONSTRUCTION COST (CONCEPTUAL) |  |  | \$170,000 |
| CONTIGENCY (20\%) | 1 | LS | \$34,000 | \$35,000 |
| DESIGN AND INSPECTION (25\%) | 1 | LS | \$42,500 | \$45,000 |
|  |  |  | FINAL TOTAL | \$250,000 |

${ }^{1}$ INCLUDES TYPICAL COST FOR CONTROLLER, SIGNAL POLES, LOOPS, WIRING, SIGNAL HEADS, ETC., FOR AN ACTUATED TRAFFIC SIGNAL.

SINGLE LANE ROUNDABOUT (120 FT DIAMETER)

| DESCRIPTION | TOTAL QUANTITY | UNIT | UNIT PRICE | TOTAL COST |
| :---: | :---: | :---: | :---: | :---: |
| SINGLE LANE ROUNDABOUT ${ }^{2}$ | 1 | EA | \$750,000 | \$750,000 |
| UTILITY RELOCATION ${ }^{3}$ | 0 | EA | \$75,000 | \$0 |
| STORMWATER AND TREATMENT ${ }^{4}$ | 1 | LS | \$175,000 | \$175,000 |
| WETLAND MITIGATION | 1 | LS | \$75,000 | \$75,000 |
| WORK ZONE TRAFFIC CONTROL | 1 | LS | \$150,000 | \$150,000 |
|  | ESTIMATED CONSTRUCTION COST (CONCEPTUAL) |  |  | \$1,150,000 |
| RIGHT OF WAY | 0 | ACRE | \$340,000 | \$0 |
| CONTIGENCY (20\%) | 1 | LS | \$230,000 | \$230,000 |
| DESIGN AND INSPECTION (25\%) | 1 | LS | \$287,500 | \$290,000 |
|  |  |  | FINAL TOTAL | \$1,670,000 |

${ }^{2}$ INCLUDES TYPICAL COST FOR PAVEMENT, CURB, EARTHWORK, DRAINAGE, LANDSCAPING, ETC., FOR A SINGLE LANE ROUNDABOUT.
${ }^{3}$ ELECTRIC AND GAS RELOCATIONS ARE ASSUMED NO COST FOR MUNICIPAL PROJECTS. WATER AND SEWER RELOCATIONS ARE NOT PRESENT.
${ }^{4}$ IMPACTS OVER 5,000 SF WITHIN DEP WATERSHEDS REQUIRE POST STORMWATER TREATMENT. \$175,000 ALLOWANCE FOR EXTRA ROW OR WORK REQUIRED.



[^0]:    ${ }^{4}$ INCLUDES TYPICAL COST FOR PAVEMENT, CURB, EARTHWORK, DRAINAGE, LANDSCAPING, ETC., FOR A FOUR WAY INTERSECTION.
    ${ }^{5}$ INCLUDES TYPICAL COST FOR PAVEMENT, CURB, EARTHWORK, DRAINAGE, LANDSCAPING, ETC., FOR A COMMERICAL PARKING LOT.
    ${ }^{6}$ ELECTRIC AND GAS RELOCATIONS ARE ASSUMED NO COST FOR MUNICIPAL PROJECTS. WATER AND SEWER RELOCATIONS ARE NOT PRESENT.
    ${ }^{7}$ IMPACTS OVER 5,000 SF WITHIN DEP WATERSHEDS REQUIRE POST STORMWATER TREATMENT. \$175,000 ALLOWANCE FOR EXTRA ROW OR WORK REQUIRED.

[^1]:    Intersection Summary

[^2]:    Intersection Summary

